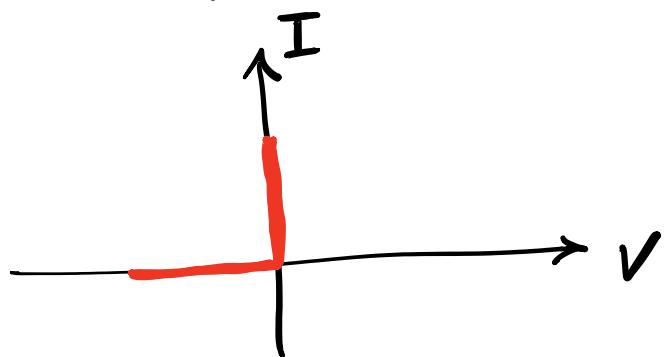


## Diode behaviour

There are three approaches to model a diode:

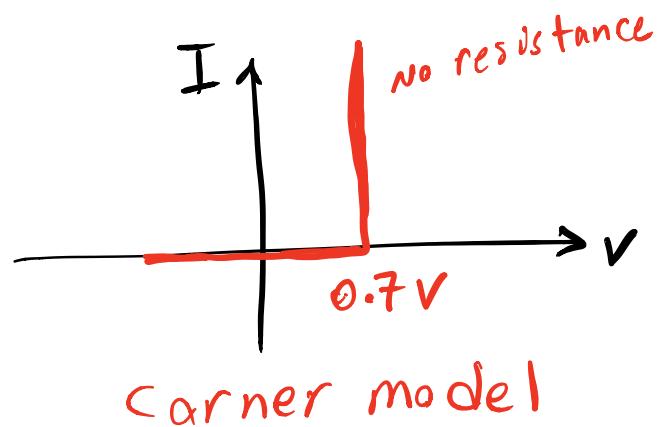
- Ideal model
- Corner model
- Real model

For the one way (ideal) model, the bulk resistance ( $r_B$ ) and the threshold voltage ( $V_D$ ) is negligible.

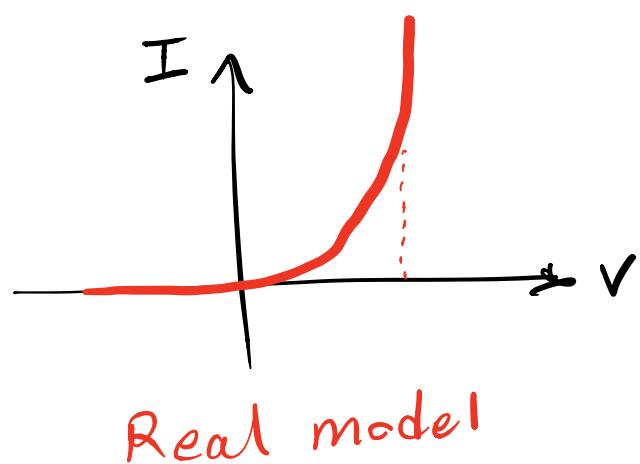


Ideal model

For the corner model  $V_D$  exists.  
But there are some simplifications:



The real model includes bulk resistance  
and voltage  $V_D$ .



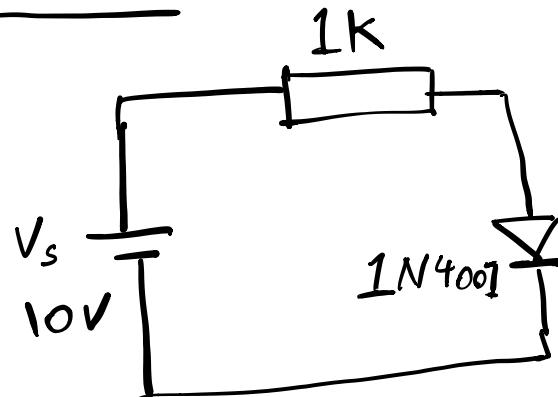
Example for ideal model:

Use an ideal model

to calculate

the load current,

voltage, power, diode power, and total power.



$$I_L = \frac{V_s}{R_L} = \frac{10V}{1\text{ K}\Omega} = 10 \text{ mA} = \frac{10}{1000} \text{ A}$$

$$V_L = 10 \text{ V} \quad \leftarrow \quad V_L = V_R + V_D$$

$V_D = 0$  in ideal model

$$P_L = V_L \times I_L = 10 \times \frac{10}{1000} \text{ A} = 0.1 \text{ Watt}$$

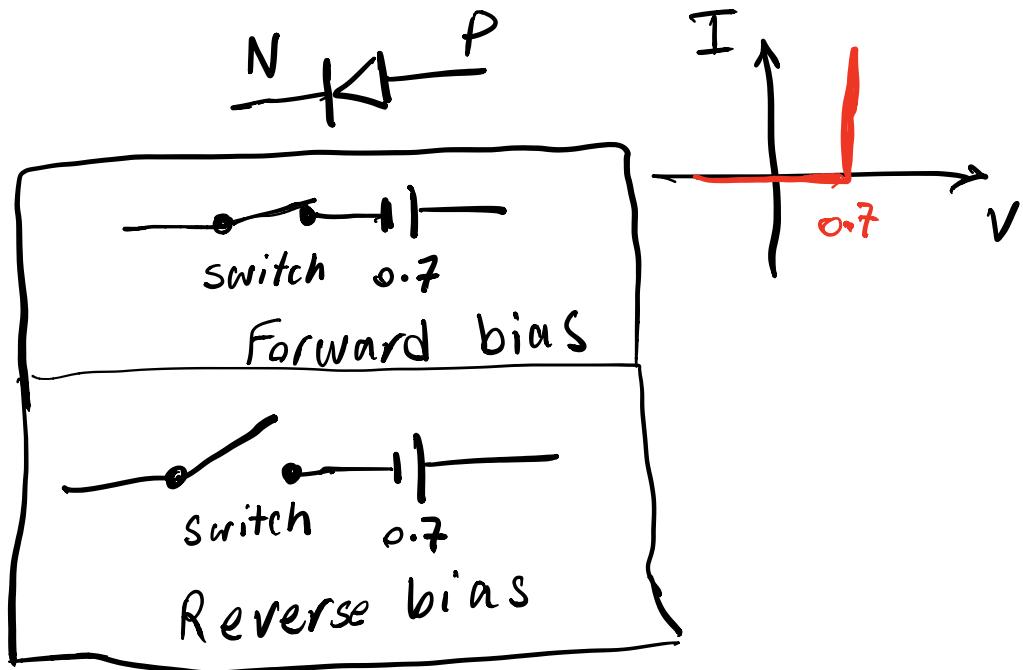
$$P_D = V_D \times I_L = 0 \times I_L = 0 \text{ Watt}$$

$$P_T = P_L + P_D = 0.1 + 0 = 0.1 \text{ Watt}$$

## Corner Model

The corner model can be simulated using a power supply ( $0.7V$ ) and switch with zero resistance.

The switch is closed in the forward bias, and open in the reverse biasing:

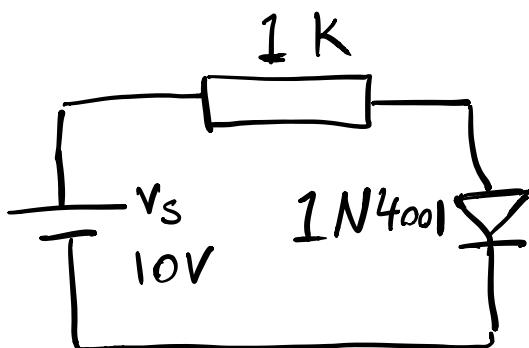


## Example

use the corner model to calculate the load current, voltage, power, diode power and total power.

$$I_L = \frac{(V_s - V_D)}{R_L}$$

$$= \frac{(10 - 0.7)}{1 \text{ k}\Omega} = 9.3 \text{ mA}$$



$$V_L = I_L R_L = 9.3 \text{ mA} \times 1 \text{ k}\Omega = 9.3 \text{ V}$$

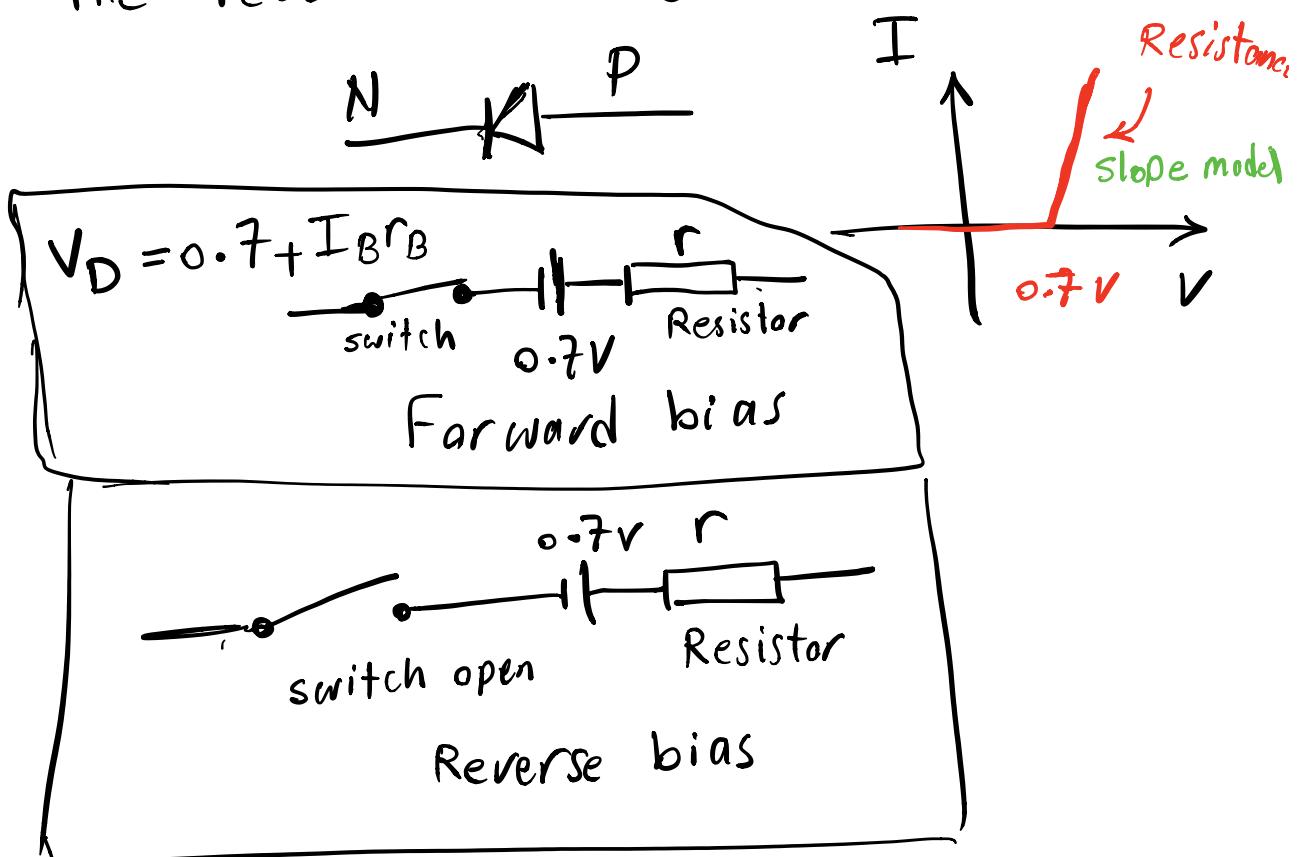
$$P_L = V_L I_L = 9.3 \times 9.3 \text{ mA} = 86.5 \text{ mW}$$

$$P_D = V_D I_L = 0.7 \times 9.3 \text{ mA} = 6.51 \text{ mW}$$

$$\underline{P_T = P_L + P_D = 6.51 + 86.5 = 93 \text{ mW}}$$

## Real model

The real model can be simulated using a power supply ( $0.7V$ ), serial resistor and switch. The switch is closed in the forward bias, and open in the reverse bias.



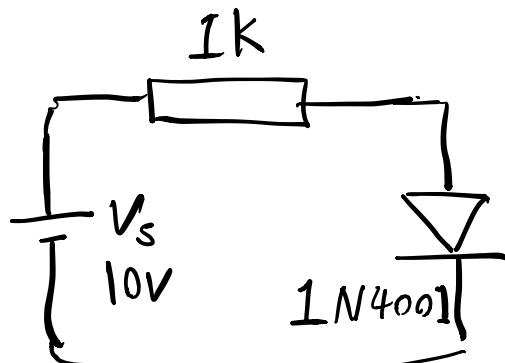
## Example

use the slope model to calculate the load current, voltage, power, diode power, and total power.

The 1N4001 diode has a bulk resistance of 0.23 ohm.

$$I_L = \frac{(V_S - V_D)}{(R_L + r_B)} = \frac{10 - 0.7}{1k - 0.23}$$

$$I_L = 9.3 \text{ mA}$$



$$V_L = I_L \times R_L = 9.3 \text{ mA} \times 1\text{k} = 9.3 \text{ V}$$

$$P_L = V_L \times I_L = 9.3 \times 9.3 \text{ mA} = 86.5 \text{ mW}$$

$$V_D = 0.7 + (9.3 \text{ mA} \times 0.23) = 0.702 \text{ V}$$

$$P_D = V_D \times I_L = 0.702 \times 9.3 \text{ mA} = 6.53 \text{ mW}$$

$$P_T = P_L + P_D = 6.53 + 86.5 = 93.03 \text{ mW}$$

---

which model should I use?

- In troubleshooting or preliminary analysis when large error is acceptable use ideal model.
- If the circuit uses precision resistors ( $\pm 1\%$ ), real model should be used (However, corner model approximation is acceptable)

The following formula can be used for calculating the diode current.

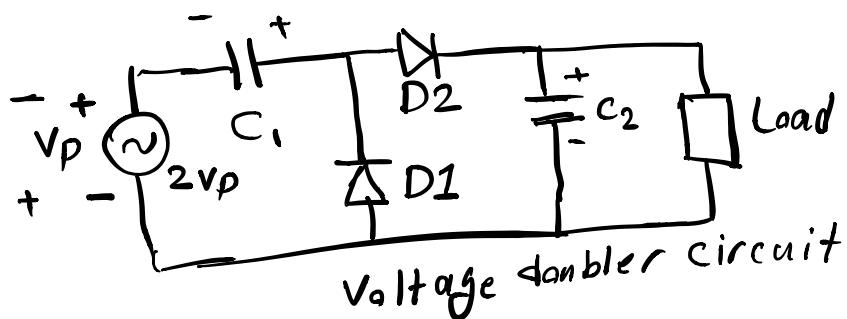
$$I_F = \frac{(V_S - 0.7)}{r_B + R_L}$$

---

### Applications of Diodes:

#### — Voltage doubler:

To understand the operation of the circuit, we need to look at the half-cycles of the ac input.



During the first negative half-cycle, D1 will be forward biased and will

hold the right end of  $C_1$  at ground.

During the following positive half cycle,

$D_1$  will be reverse biased and therefore will not conduct current. The

voltage on  $C_1$  will add to the output voltage, so  $2V_p$  appear at the left end of  $D_2$ . Since  $C_2$  is

not yet charged, this will forward bias  $D_2$  and allow the voltage

at the right end of  $C_1$  to be applied to the top of  $C_2$ .

$C_2$  will charge as  $C_1$  discharges.

until the two capacitors can no longer forward-bias  $D_2$ . For the

first positive half-cycle, the

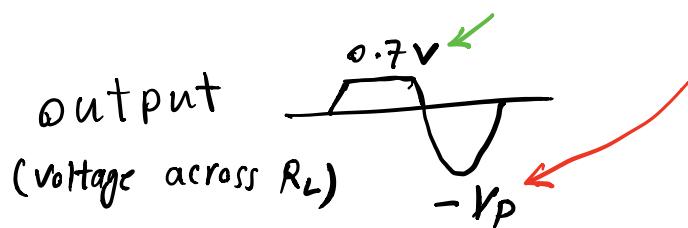
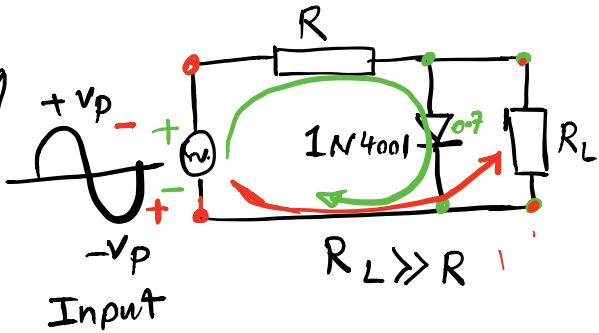
voltage  $C_2$  will be equal to  $V_p$

and  $C_1$  will be completely discharged.

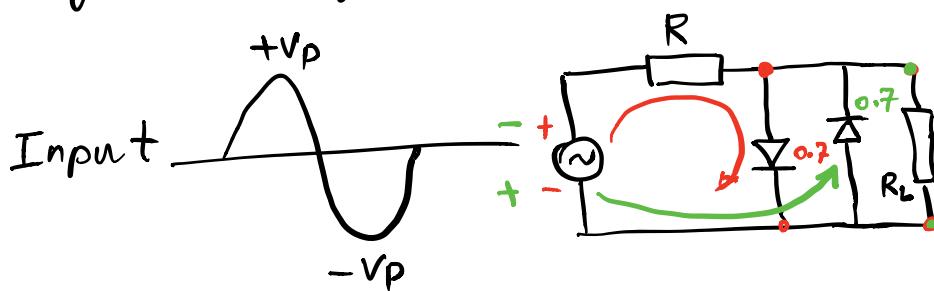
---

## - Limiters

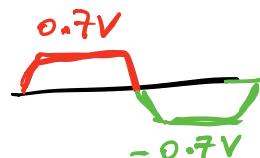
Positive voltage limiter



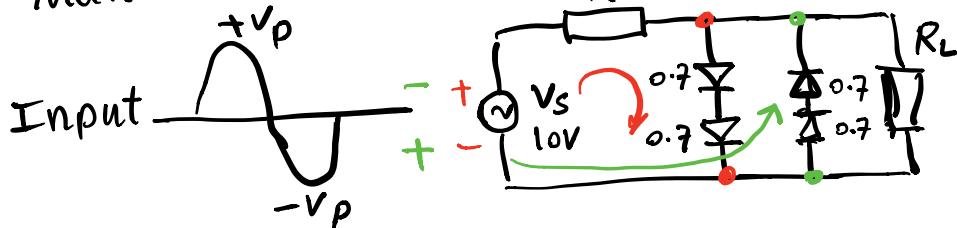
Negative voltage limiter



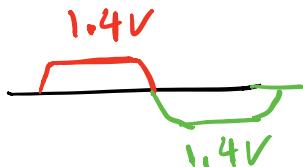
The output voltage across  $R_L$



Multilimiter



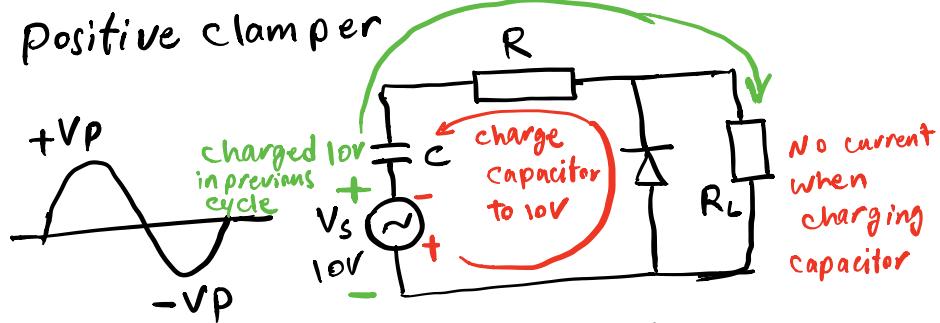
The voltage across  $R_L$



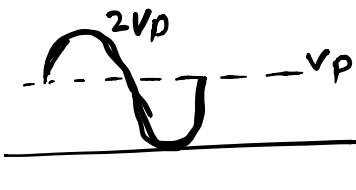
### Clampers

Diode clampers add a DC level to an AC signal and are sometimes known as dc restorers.

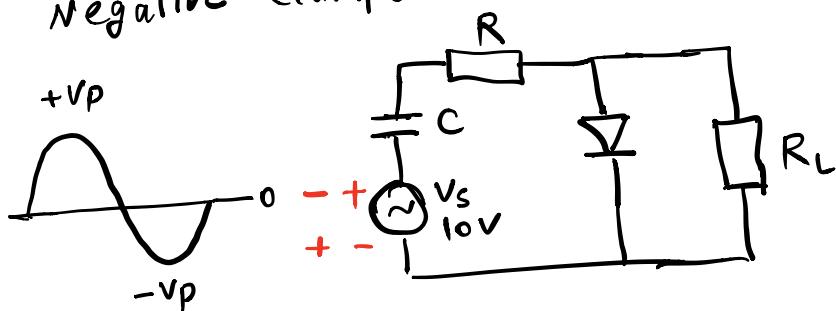
#### positive clamer



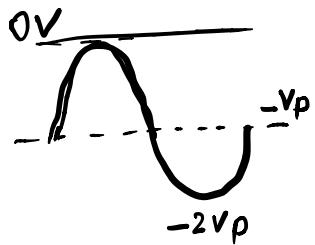
#### The voltage output



#### negative clamer



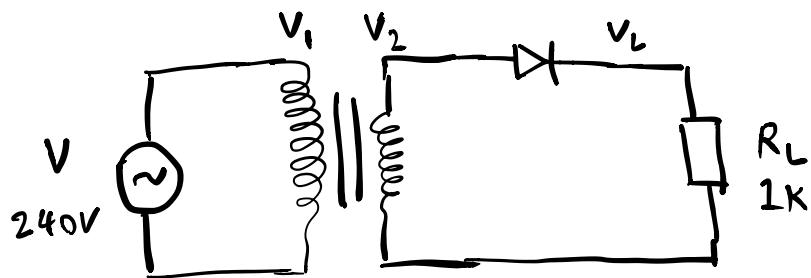
Voltage across the  $R_L$



## Rectifiers

A half wave rectifier is special case of a clipper. In half-wave rectification, either the positive or negative half of the AC wave is passed easily, while the other half is blocked, depending on the polarity of the rectifier.

Because only one half of the input waveform reaches the output, it is very inefficient if used for power transfer. Half wave rectification can be achieved with a single diode in a one phase supply.



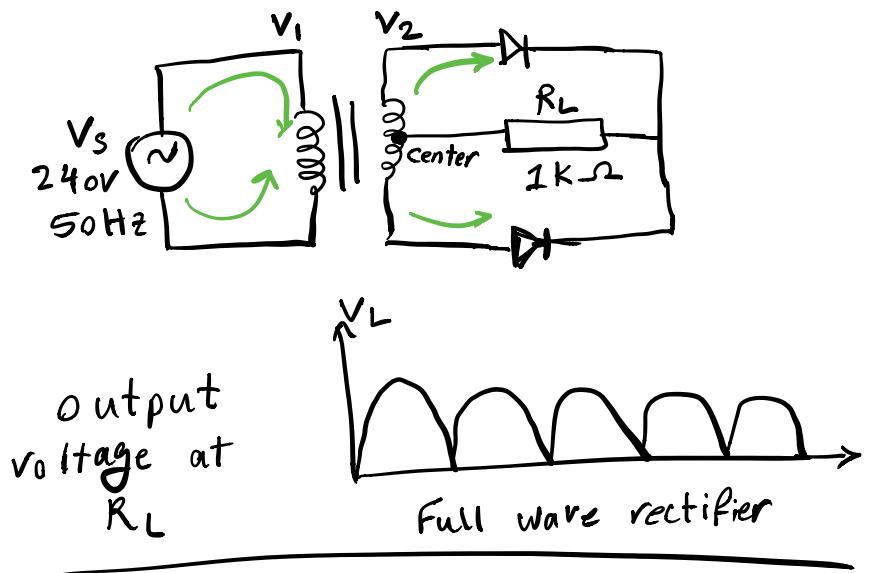
$$V_2 = V_1 \left( N_2 / N_1 \right) \quad I_2 = I_1 \left( \frac{N_1}{N_2} \right)$$


---

### Full wave rectifier

A Full wave rectifier converts the whole of the input waveform to one of constant polarity (positive or negative) at its output by reversing the negative (or positive) portions of the alternating current waveform.

The positive (or negative) portions thus combine with the reversed negative (positive) portions to reduce an entirely positive (negative) voltage/current waveform.



### Bridge Rectifier

Full wave rectification converts both polarities of the input waveform to DC, and is more efficient. However, in a circuit with a non-center tapped transformer, four rectifiers required instead of the one needed for half-wave rectification.

