

Instrumentation and Controls

ETM 3301

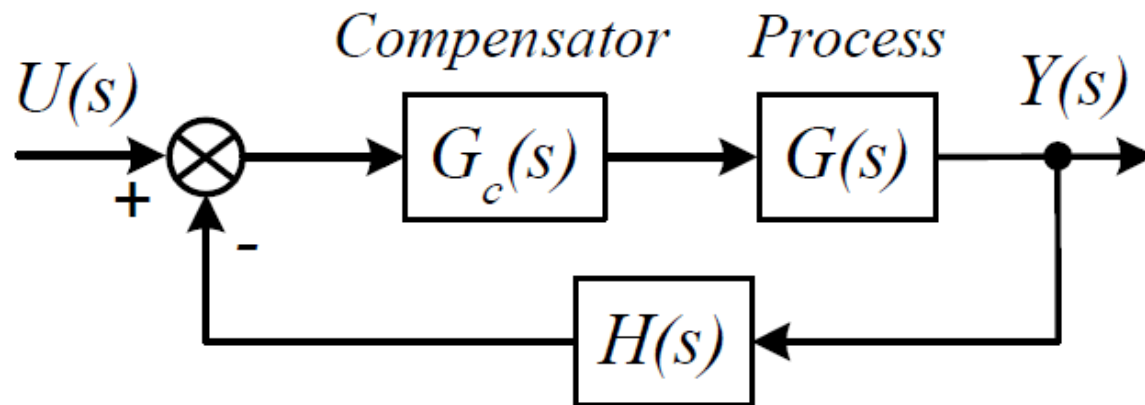
Lecture 26

Instructor

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Cascade Compensation

- *Control system design*: the arrangement of the system structure and the selection of suitable components and parameters.
- *Compensation*: the alteration or adjustment of a control system in order to provide the required performance.
- *Compensator*: is an additional component that is inserted into a control system to compensate for a deficient performance.



The insertion of a compensator can increase Phase Margin.

Phase Lead Compensator

Transfer
function

$$G_c(s) = \frac{1 + \alpha Ts}{1 + Ts} \quad (\alpha > 1)$$

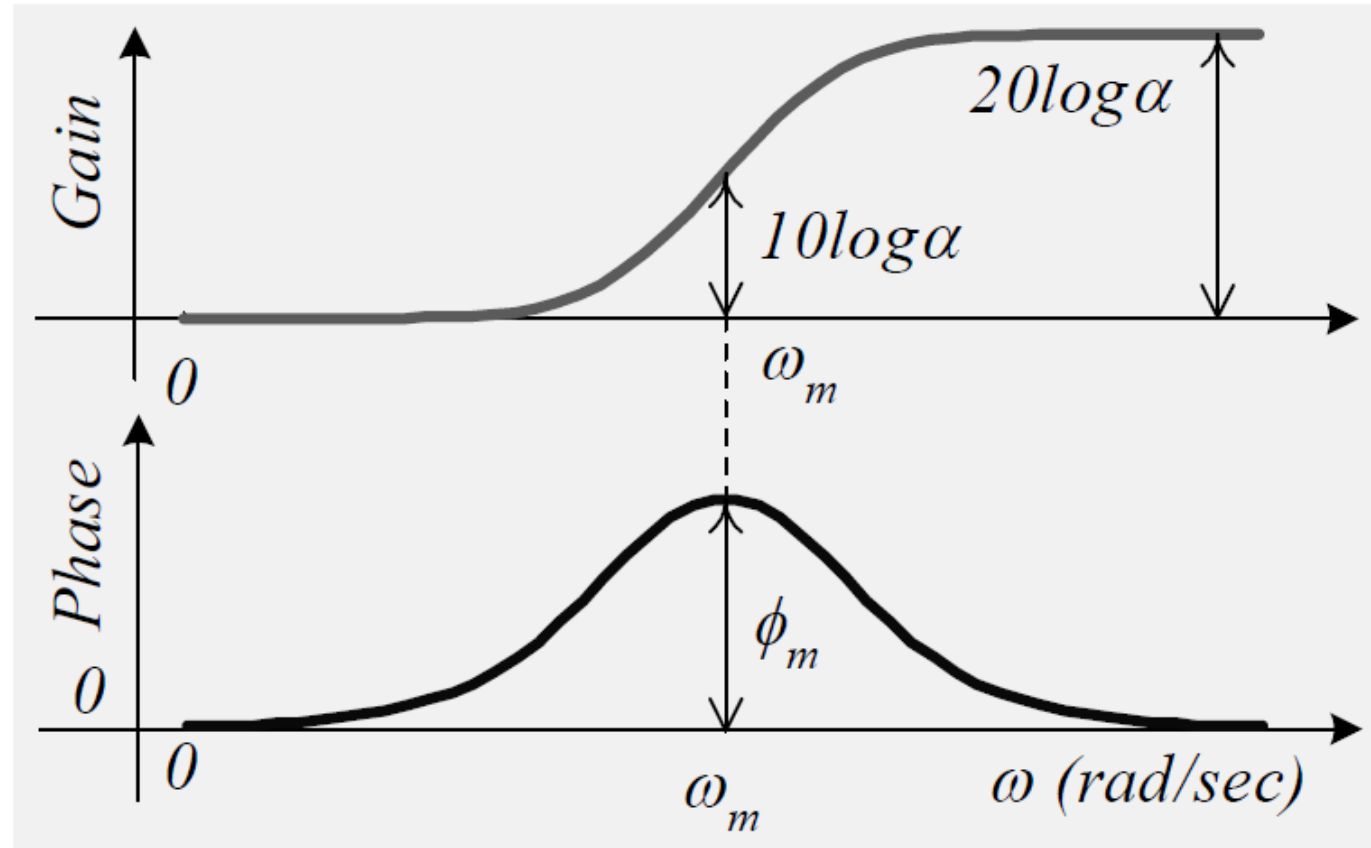
$$G_c(j\omega) = \frac{1 + \alpha Tj\omega}{1 + Tj\omega}$$

$$|G_c(j\omega)| = \frac{\sqrt{1 + (\alpha T\omega)^2}}{\sqrt{1 + (T\omega)^2}}$$

$$\angle G_c(j\omega) = \tan^{-1} \alpha T\omega - \tan^{-1} T\omega > 0$$

$$\begin{aligned} \text{gain} &= 20 \log_{10} |G_c(j\omega)| = 20 \log_{10} \frac{\sqrt{1 + (\alpha T\omega)^2}}{\sqrt{1 + (T\omega)^2}} \\ &= 20 \log_{10} \sqrt{1 + (\alpha T\omega)^2} - 20 \log_{10} \sqrt{1 + (T\omega)^2} \\ &= 10 \log_{10} (1 + (\alpha T\omega)^2) - 10 \log_{10} (1 + (T\omega)^2) \end{aligned}$$

Phase Lead Compensator



- The maximum value of phase lead occurs at the frequency ω_m :

$$\omega_m = \frac{1}{T\sqrt{\alpha}}$$

Phase Lead Compensator

- At the frequency ω_m , the maximum phase is ϕ_m

$$\sin \phi_m = \frac{\alpha - 1}{\alpha + 1}$$

gain is $\sqrt{\alpha}$ or $10\log_{10} \alpha$

- *The bigger the value of α , the bigger the maximum phase lead ϕ_m .*

Function of Phase Lead Compensator

- Compensated system OLTF: $G_c(s)G(s)$

$$\text{Gain} \quad |G_c(j\omega)| \times |G(j\omega)| \quad 20\log|G_c(j\omega)| + 20\log|G(j\omega)|$$

$$\text{Phase} \quad \angle G_c(j\omega) + \angle G(j\omega)$$

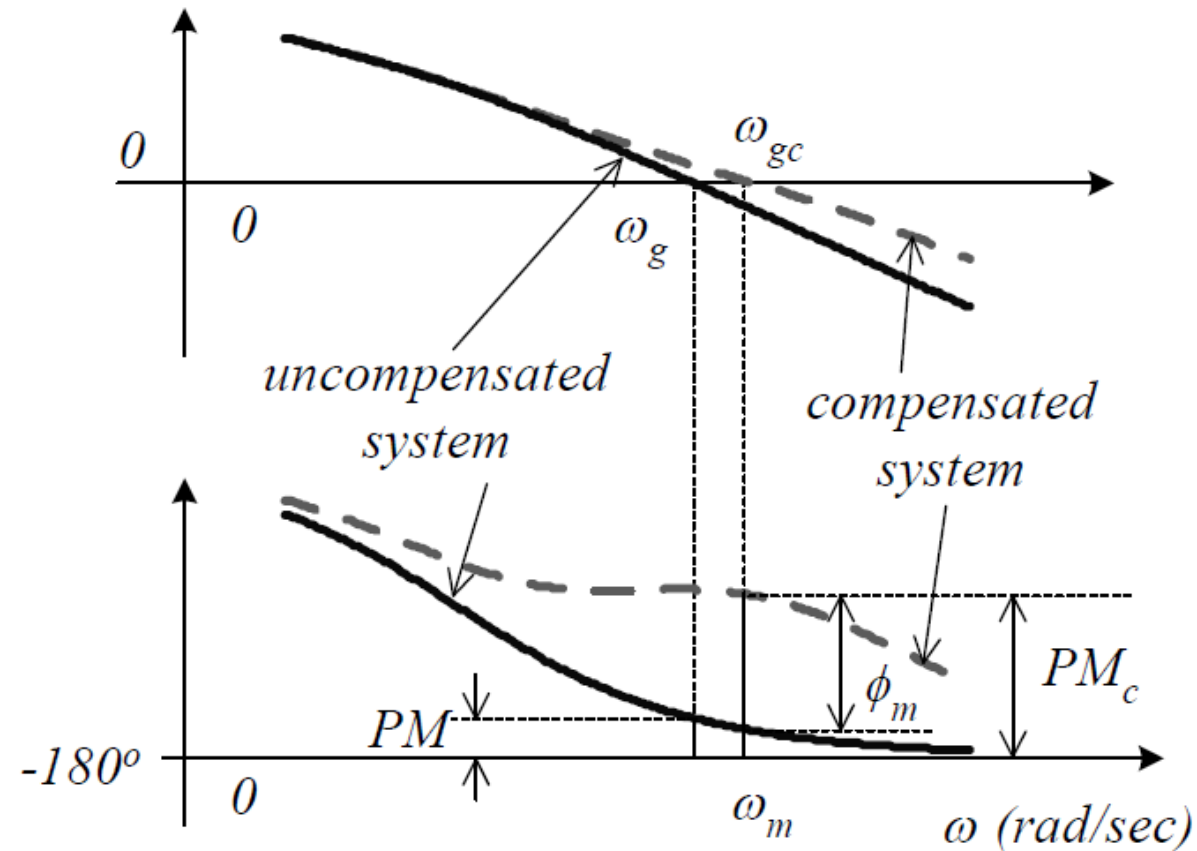
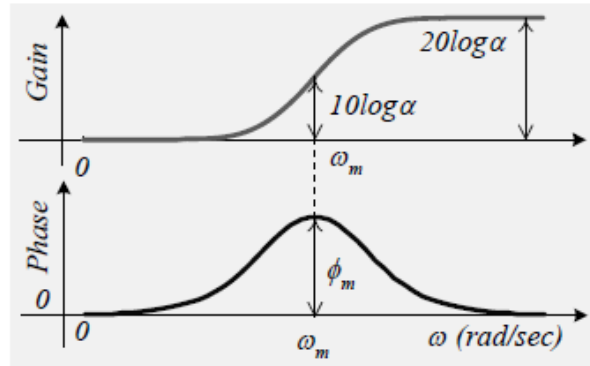
- Both gain and phase are increased, but the increase in the phase is more significant.
- The effect of a phase lead compensator when introduced into the forward path of a closed-loop control system:
 - to produce a faster and stable system by increasing the phase margin!

Phase lead compensator design principle

- To generate the maximum increase in the phase margin, the biggest phase lead (ϕ_m) must occur at the gain crossover frequency of the compensated system.

$$\omega_m = \omega_{gc}$$

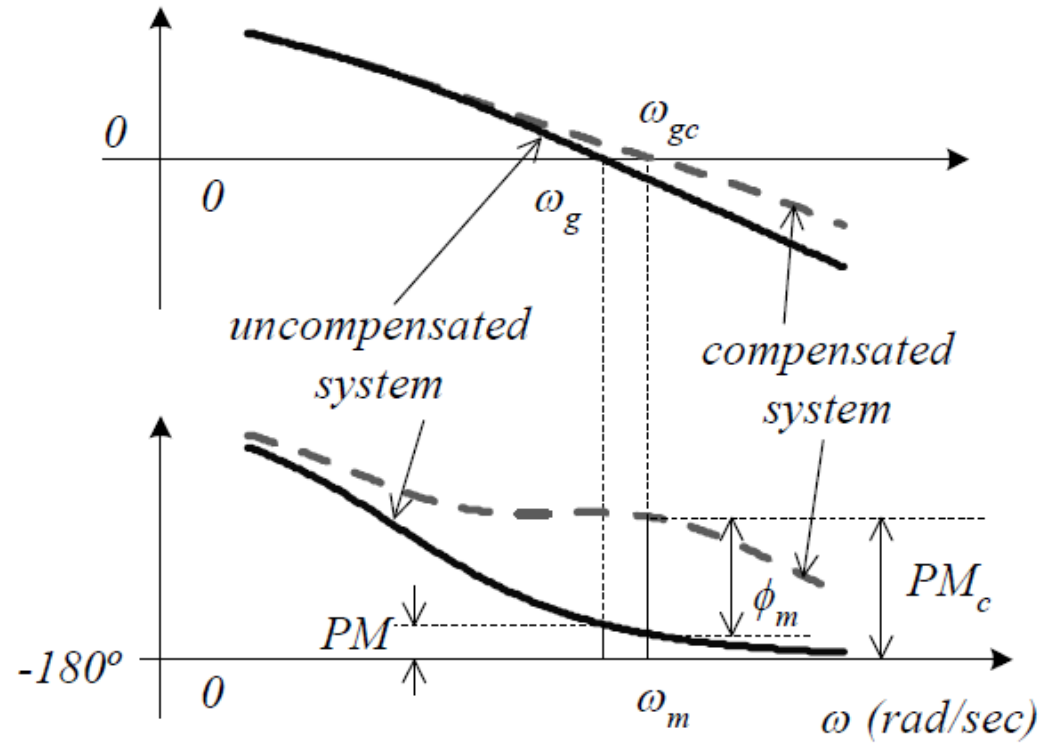
(0db frequency)



Phase lead compensator design principle

$$\omega_m = \omega_{gc}$$

(0db frequency)



compensated gain = uncompensated gain + compensator gain

at ω_m compensator gain = $10 \log \alpha$ (dB)

uncompensated gain must be $-10 \log \alpha$ (dB) at ω_m

Phase lead compensator design procedure

- Adjust the system parameter (K) to satisfy the steady state error requirement.
- Plot Bode diagram of the uncompensated system frequency response.
- Evaluate uncompensated system phase margin.
- Allowing for a small amount of safety ($\approx 10\%-30\%$), determine the necessary phase lead ϕ_m .
- Find α using equation:

$$\sin \phi_m = \frac{\alpha - 1}{\alpha + 1} \quad \Rightarrow \quad \alpha = \frac{1 + \sin \phi_m}{1 - \sin \phi_m}$$

$$G_c(s) = \frac{1 + \alpha Ts}{1 + Ts} \quad (\alpha > 1)$$

Phase lead compensator design procedure

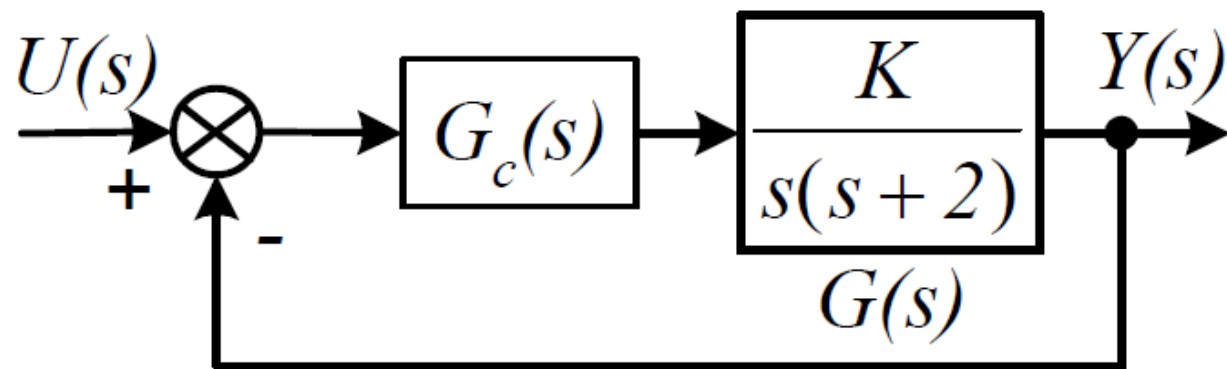
- Evaluate $10\log\alpha$ and determine the frequency where the uncompensated gain (magnitude) curve is equal to $-10\log\alpha$ dB. Because the compensator provide a gain of $10\log\alpha$ at ω_m , this frequency is the new 0 dB crossover frequency and ω_m simultaneously.
- Find the value of T using equation:

$$\omega_m = \frac{1}{T\sqrt{\alpha}} \Rightarrow T = \frac{1}{\omega_m\sqrt{\alpha}}$$

- Plot the compensated system frequency response and check the phase margin, repeat the design if necessary.

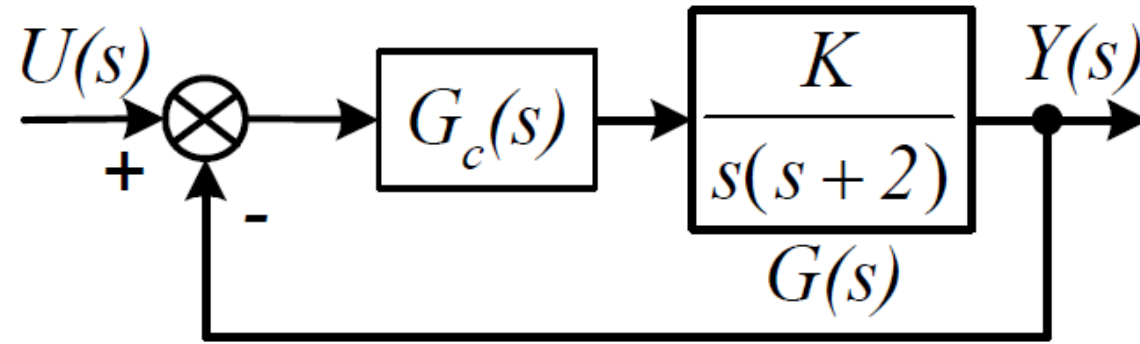
Phase-Lead Compensator Design Example

- For the system with the following block diagram



- find the parameter K to make the system have 5% steady state error for an unit ramp input.
- design the compensator $G_c(s)$ to provide the phase margin of 45° .

Phase-Lead Compensator Design Example



- The steady state error for a unit ramp input is:

$$e_{ss} = \frac{1}{K_V} \quad K_V = \lim_{s \rightarrow 0} s [G_c(s)G(s)]$$

$$K_V = \lim_{s \rightarrow 0} s \left[\frac{1 + \alpha Ts}{1 + Ts} \frac{K}{s(s+2)} \right] = \frac{K}{2}$$

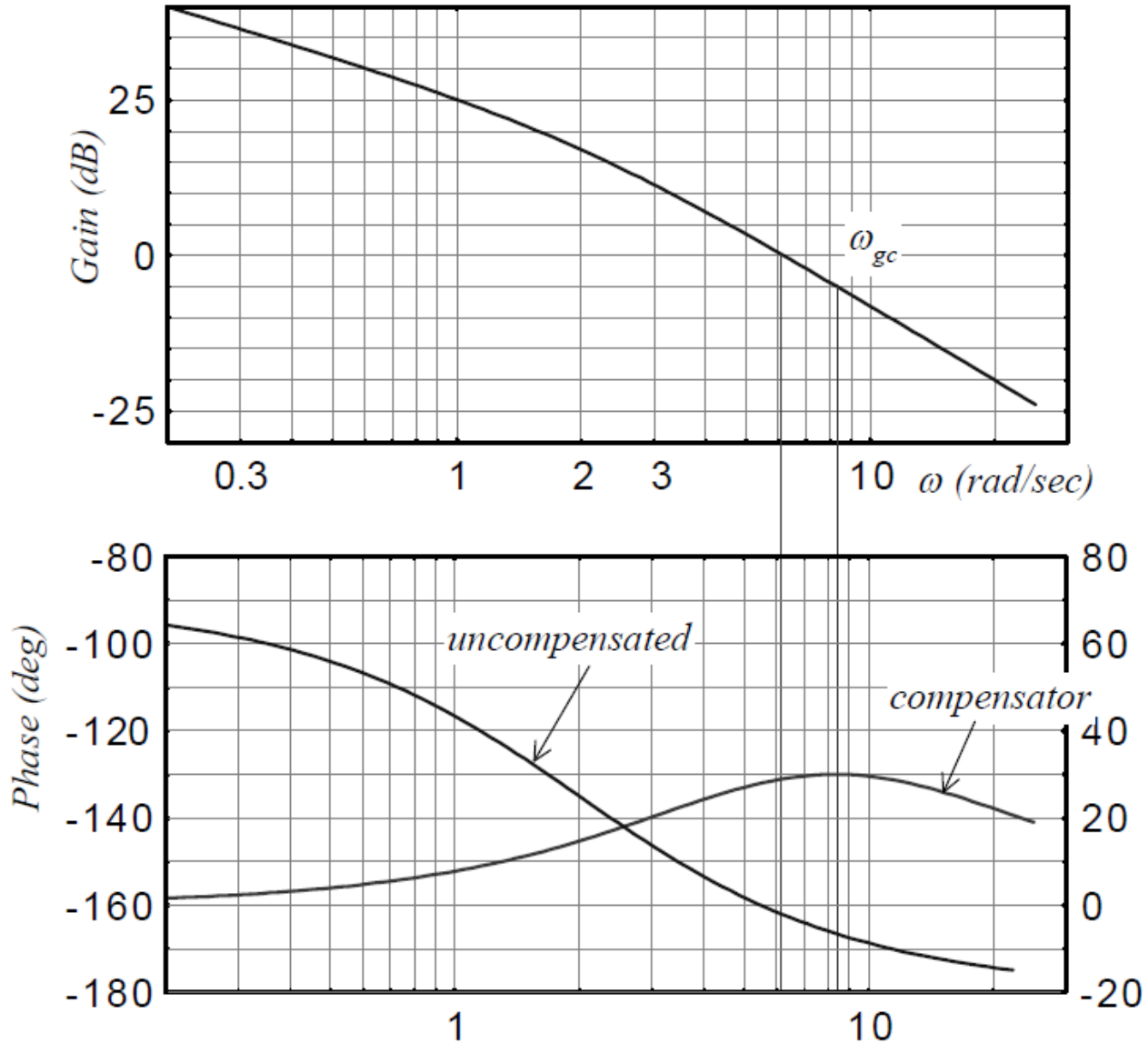
$$e_{ss} = \frac{2}{K} = 0.05 \quad \Rightarrow \quad K = 40 \quad G(s) = \frac{40}{s(s+2)}$$

Phase-Lead Compensator Design Example

$G(j\omega)$

gain crossover
frequency ω_g
 $= 6.2 \text{ rad/s}$

phase margin
 $PM = 180^\circ -$
 $162^\circ = 18^\circ$



Phase-Lead Compensator Design Example

The required maximum phase lead is:

$$\phi_m = 45^\circ - 18.2^\circ + \underbrace{3^\circ}_{\text{Design safety margin}} \approx 30^\circ$$

Design safety margin

$$\frac{\alpha - 1}{\alpha + 1} = \sin \phi_m = \sin 30^\circ = 0.5 \Rightarrow \alpha = 3$$

The maximum phase lead occurs at ω_m , and this frequency will be selected so that the new gain crossover frequency ω_{gc} and ω_m coincide.

The compensator gain at ω_m is $10 \log \alpha = 4.8 \text{ dB}$.

Phase-Lead Compensator Design Example

The compensated gain crossover frequency ω_{gc} is then evaluated where the gain of the uncompensated FR $G(j\omega)$ is $-4.8dB$.

From Bode diagram, it can be found that this frequency is:

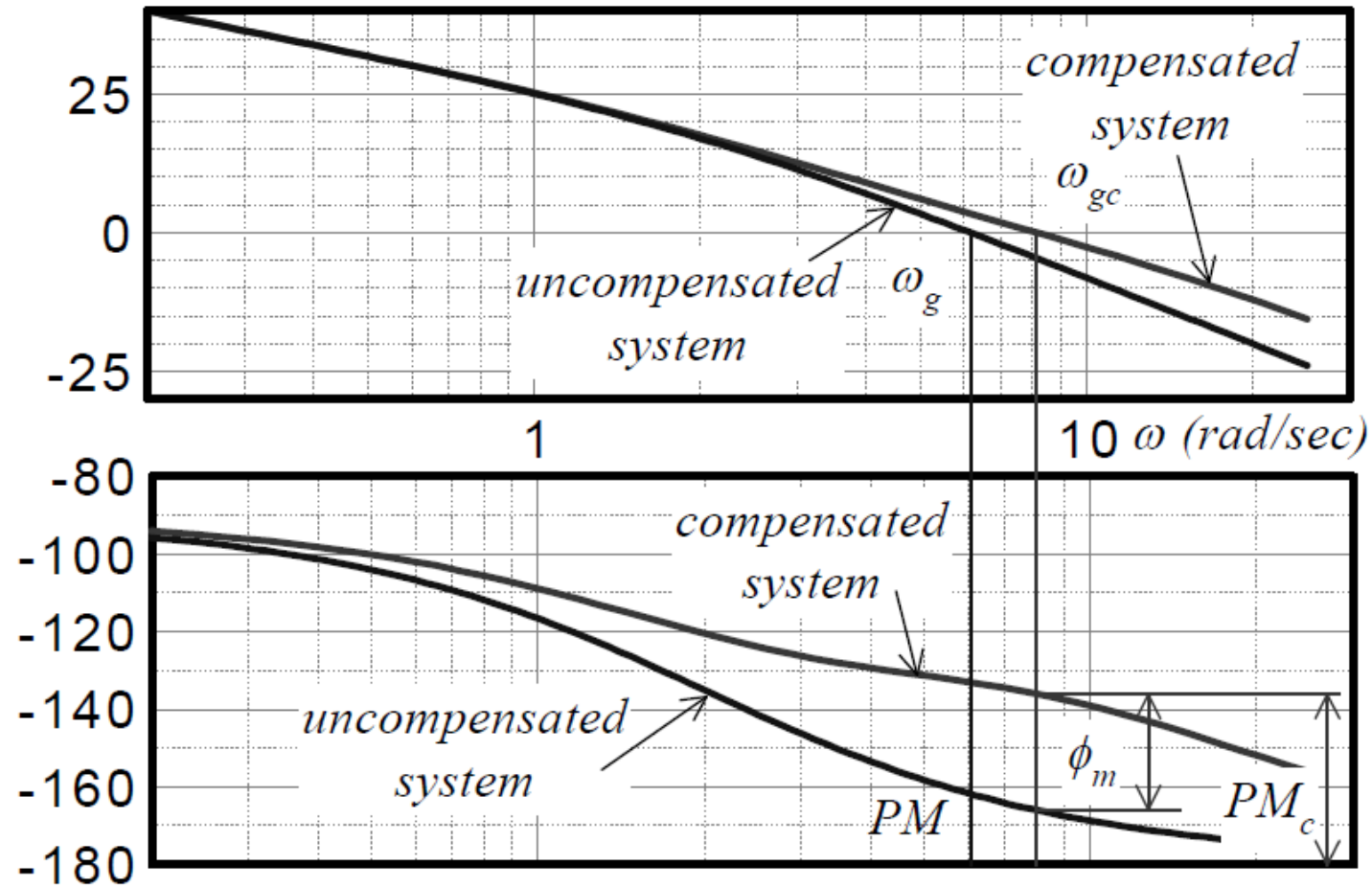
$$\omega_m = \omega_{gc} = 8.4$$

$$\omega_m = \frac{1}{T\sqrt{\alpha}} \Rightarrow T = \frac{1}{\omega_m\sqrt{\alpha}} = 0.0687$$

Finally, the compensator is $G_c(s) = \frac{1 + \alpha Ts}{1 + Ts} = \frac{1 + 0.2062s}{1 + 0.0687s}$

Compensated system
OLTF $G_c(s)G(s) = \frac{20(1 + 0.2062s)}{s(1 + 0.5s)(1 + 0.0687s)}$

Phase-Lead Compensator Design Example



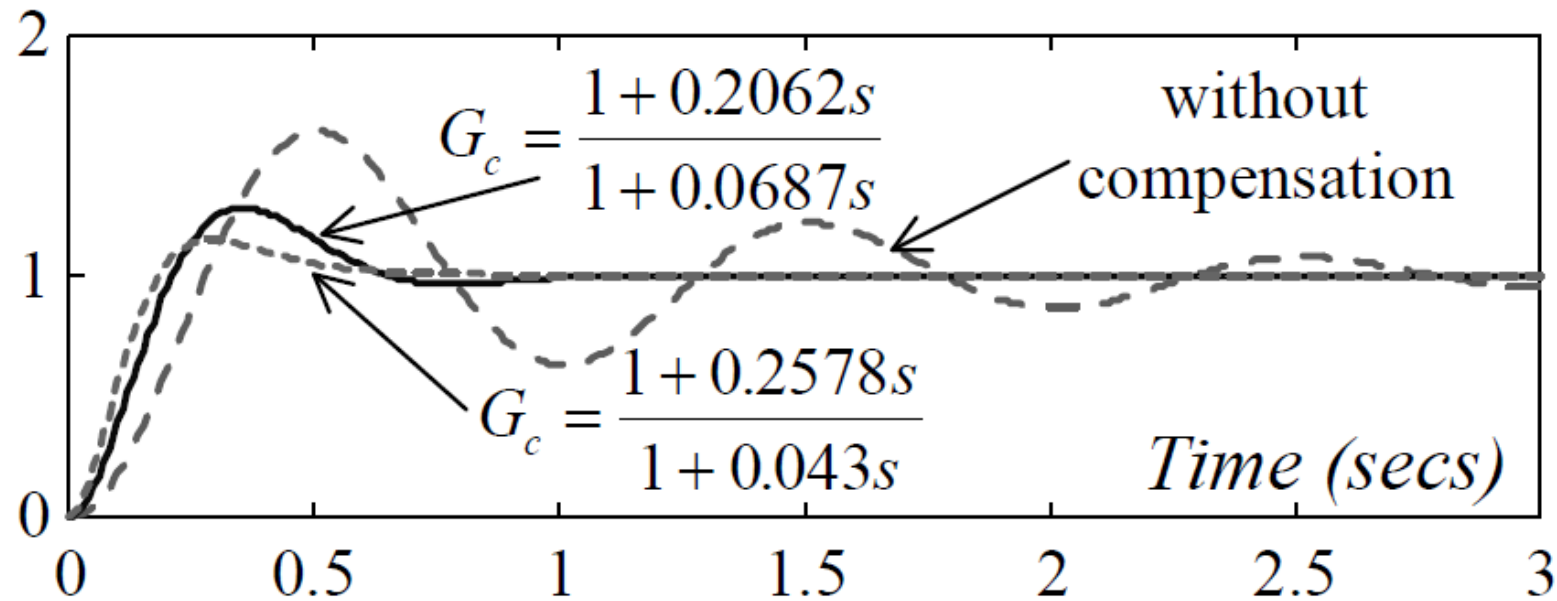
Compensated system phase margin $PM_c = 43.8^\circ$

Design requirement is not satisfied.

Phase-Lead Compensator Design Example

Further improvement can be made by increasing ϕ_m to 45° .

$$G_c = \frac{1 + 0.2578s}{1 + 0.043s} \quad PMc = 57 \quad T = 0.043 \quad \alpha = 6$$



Unit step responses of closed-loop systems.

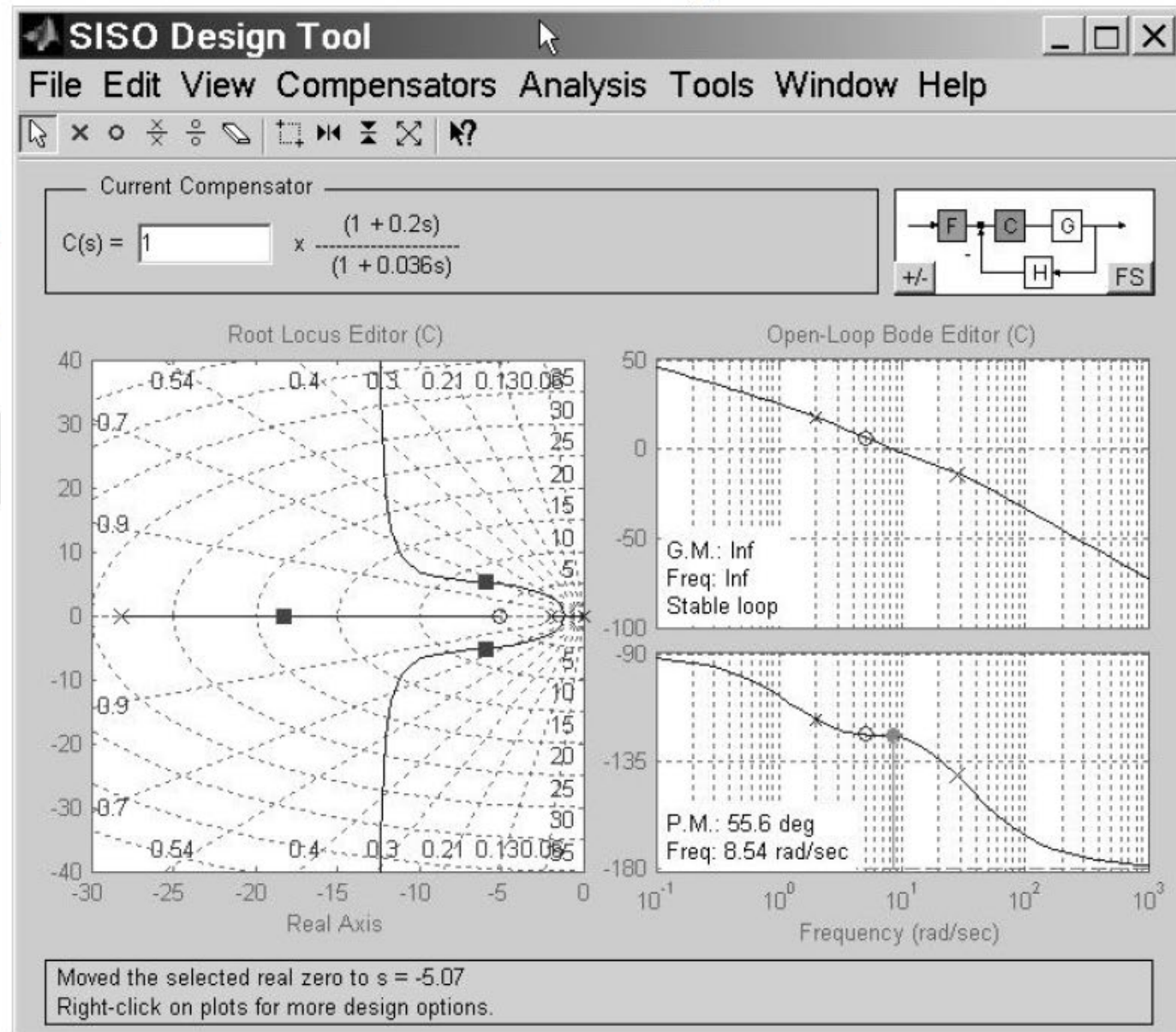
Matlab Phase-Lead Compensator

```
>>N=40;
```

```
>>D=1 2 0];
```

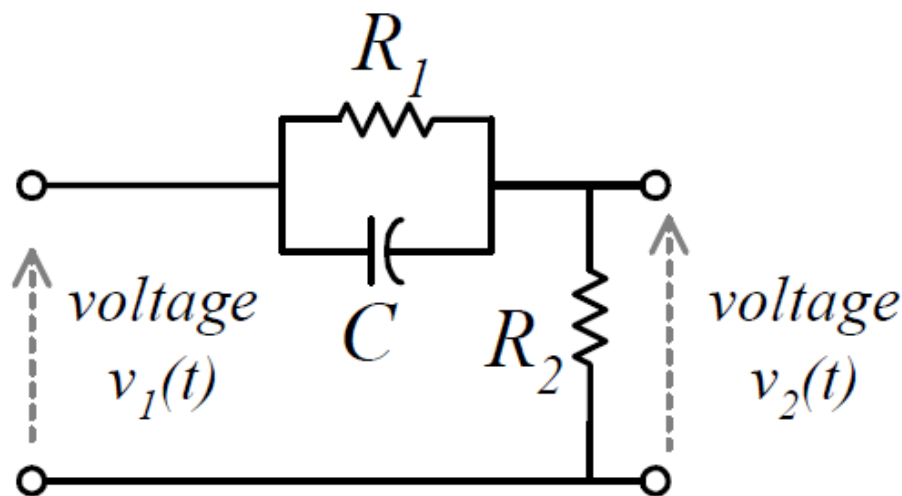
```
>>G=tf(N,D)
```

```
>>sisotool
```



Physical implementation of phase-lead compensator

The phase-lead compensator can be implemented using an electric network.



$$\begin{aligned} G_N(s) &= \frac{V_2(s)}{V_1(s)} = \frac{R_2}{R_2 + \left\{ R_1 (1/Cs) / [R_1 + 1/Cs] \right\}} \\ &= \left(\frac{R_2}{R_1 + R_2} \right) \frac{(1 + R_1 Cs)}{1 + \frac{R_1 R_2 C}{R_1 + R_2} s} \end{aligned}$$

Physical implementation of phase-lead compensator

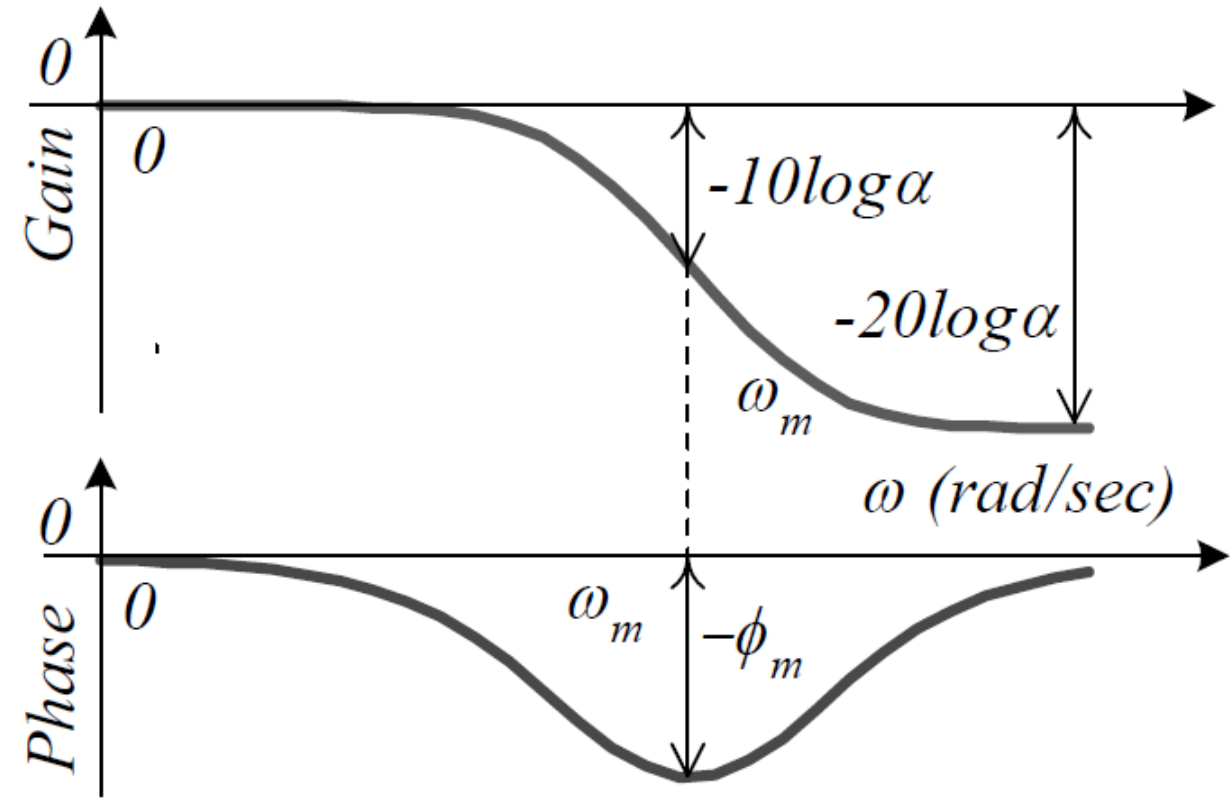
$$G_N(s) = \left(\frac{R_2}{R_1 + R_2} \right) \frac{(1 + R_1 C s)}{1 + \frac{R_1 R_2 C}{R_1 + R_2} s} \quad \text{Define:} \quad \alpha = \frac{R_1 + R_2}{R_2}$$
$$T = \frac{R_1 R_2 C}{R_1 + R_2}$$

$$G_N(s) = \left(\frac{1}{\alpha} \right) \left(\frac{1 + \alpha T s}{1 + T s} \right) \quad \text{phase lead compensator}$$

Phase lag Compensator

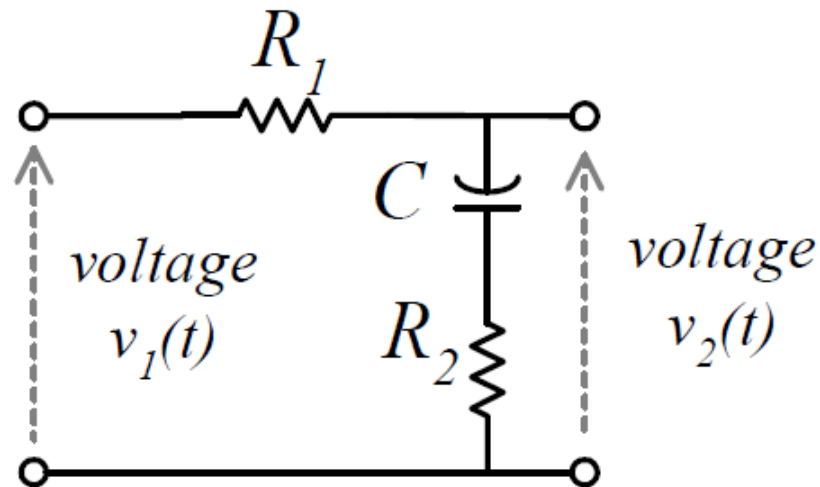
Transfer function

$$G_c(s) = \frac{1 + Ts}{1 + \alpha Ts} \quad (\alpha > 1)$$



Phase Lag Features

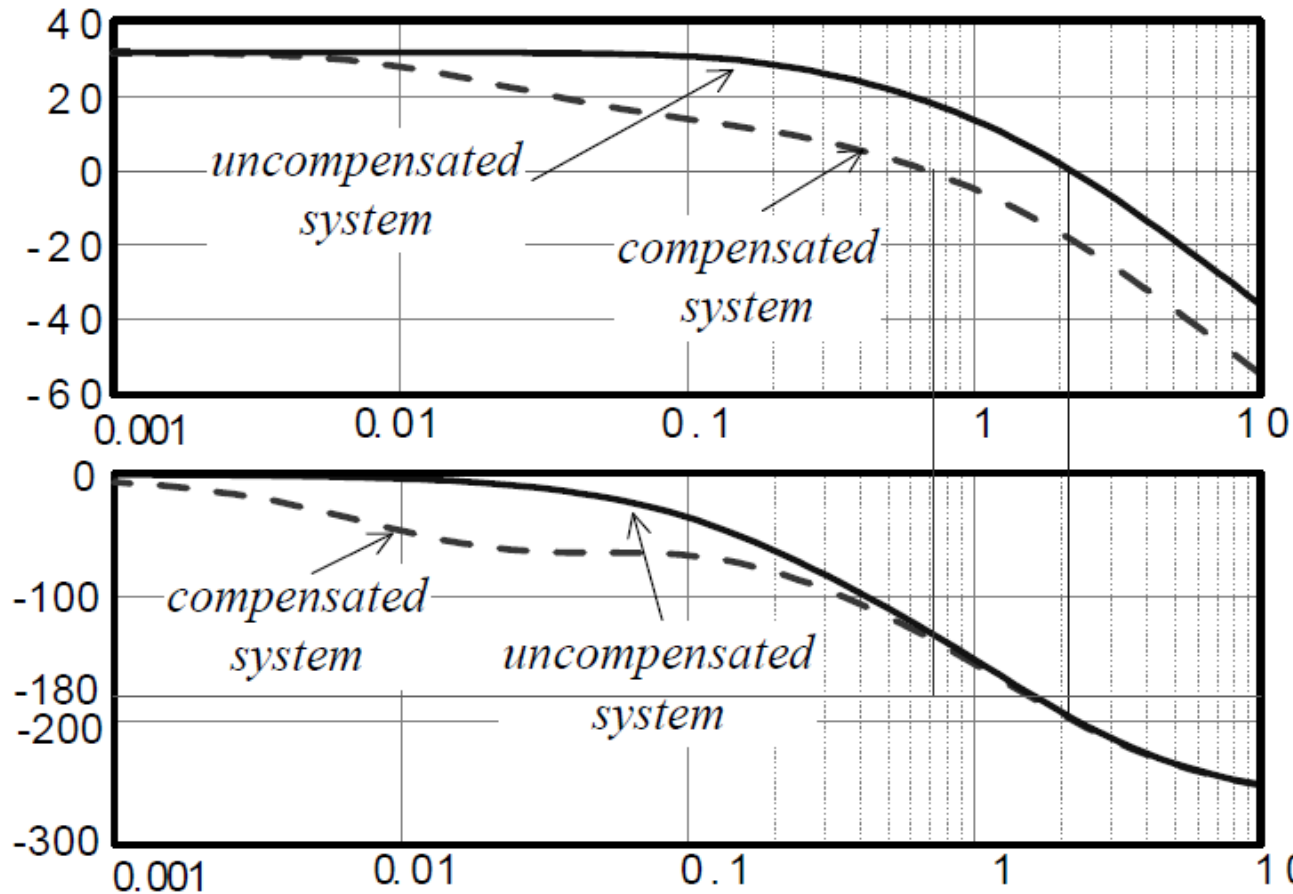
- It is a low-pass filter.
- The low frequency gain can be raised to improve the steady-state error performance.
- The high frequency gain is reduced to yield stability.
- Use it as a compensator, the gain crossover frequency can be reduced and hence the phase margin increased.



Phase-Lag Compensator Design Example

$$G(s) = \frac{40}{(1 + 5s)(1 + s)(1 + 0.5s)}$$

Uncompensated system is unstable.



By reducing gain crossover frequency, the phase margin is increased.

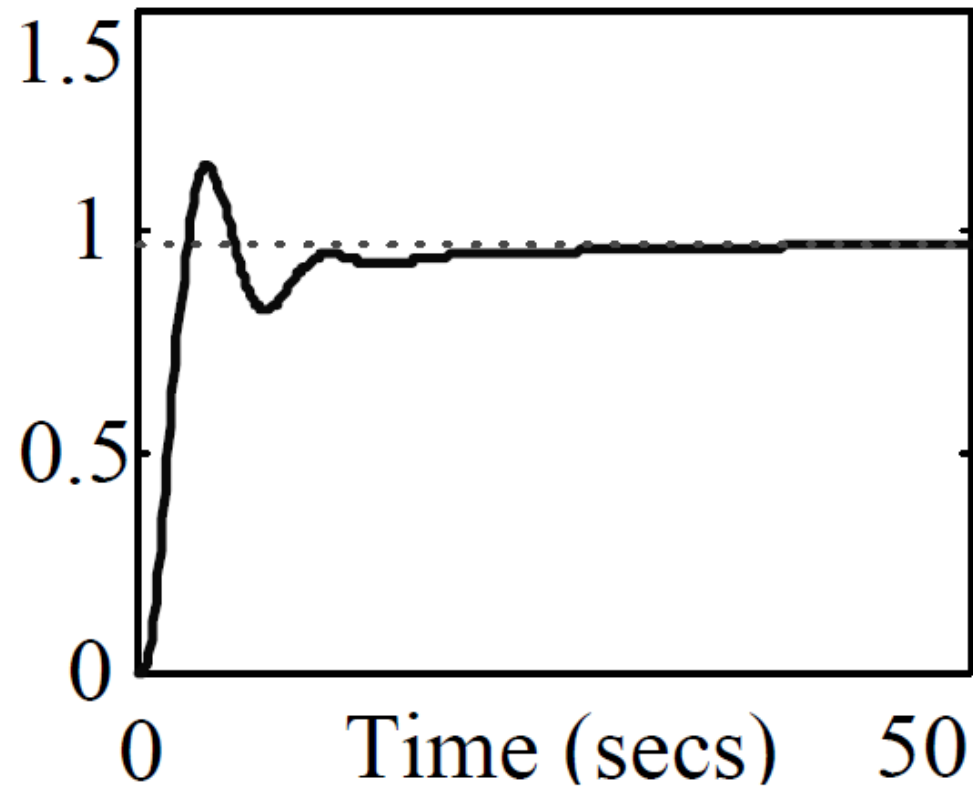
Phase-Lag Compensator Design Example

Phase lag compensator

$$G_c(s) = \frac{1 + 14s}{1 + 8.6 \times 14s}$$

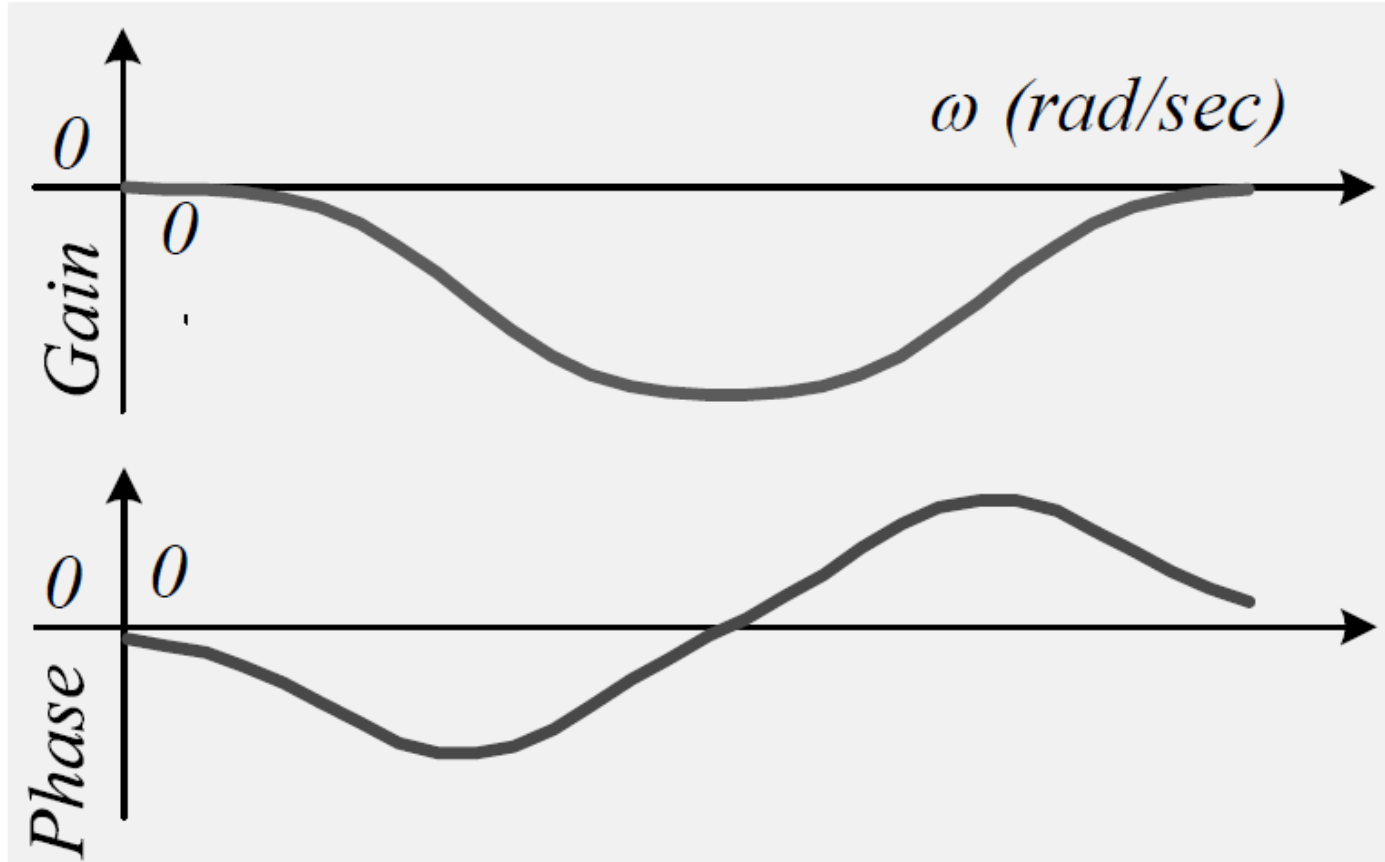
system is stabilised

step response is
satisfactory



Lag-Lead compensation

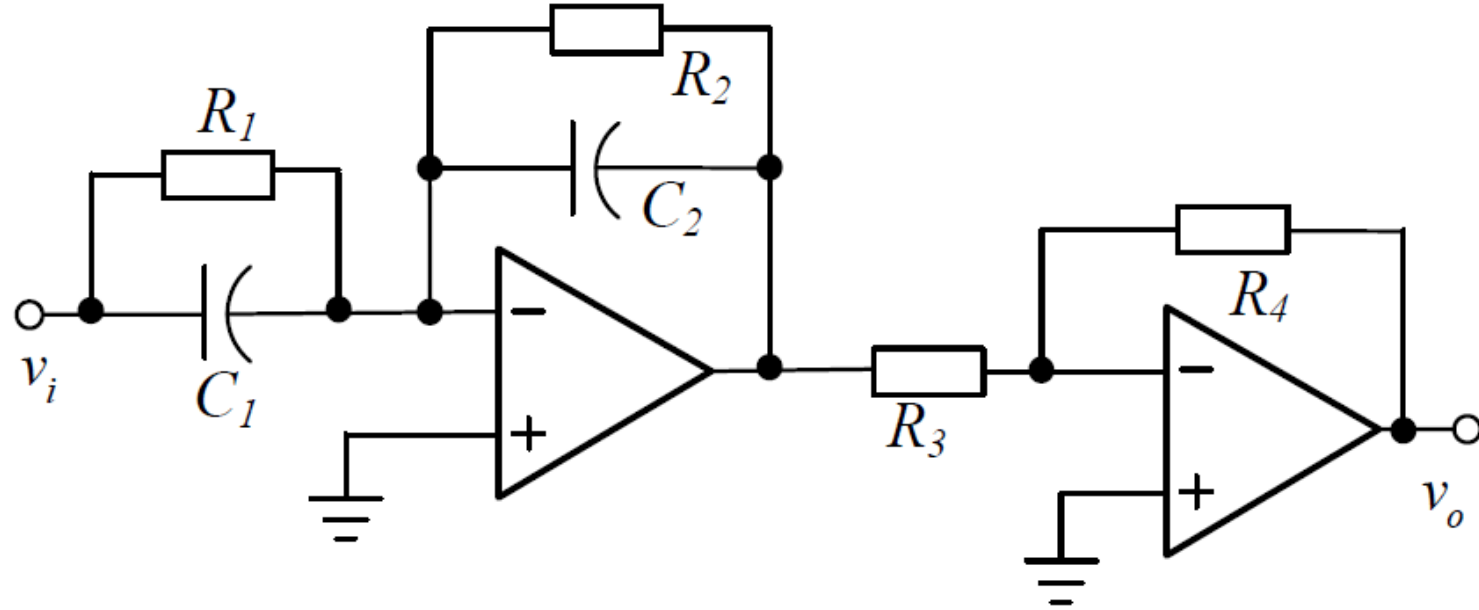
$$G_c(s) = \frac{1 + T_1s}{1 + \beta T_1s} \frac{1 + \alpha T_2s}{1 + T_2s} \quad \alpha > 1, \beta > 1, T_1 > T_2$$



Lag-Lead compensation

- Combines the advantages of phase-lag and phase-lead compensators.
- First, the lag compensator is designed to yield the proper steady-state performance with the improved stability.
- Next, the lead compensator is designed to speed up the transient response.

Implement Phase Lead/Lag Compensator using Operational Amplifiers



$$\frac{V_o(s)}{V_i(s)} = \left(-\frac{\frac{R_2}{1 + R_2 C_2 s}}{\frac{R_1}{1 + R_1 C_1 s}} \right) \left(-\frac{R_4}{R_3} \right) = \frac{R_4 R_2 (1 + R_1 C_1 s)}{R_3 R_1 (1 + R_2 C_2 s)}$$

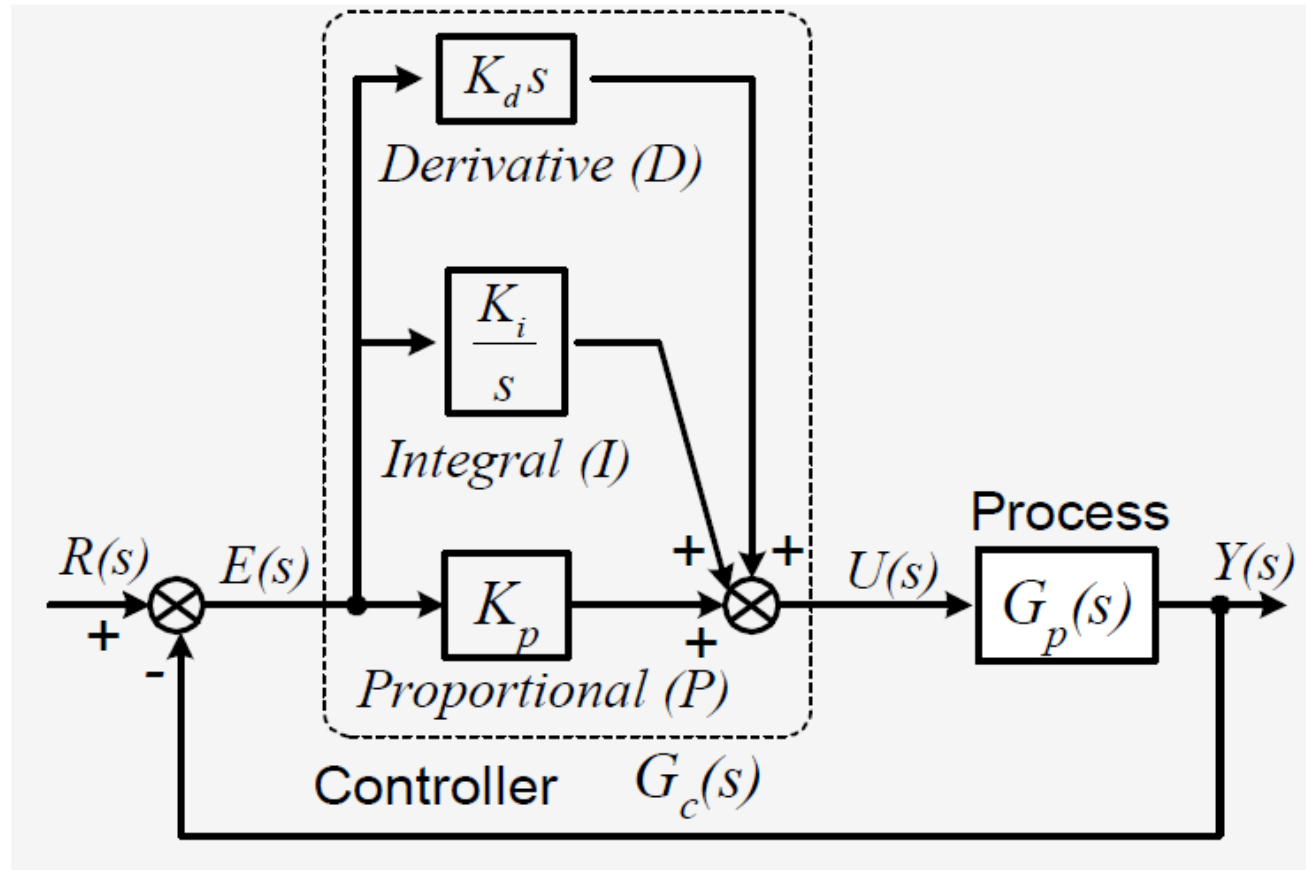
$R_1 C_1 > R_2 C_2$: phase lead

$R_1 C_1 < R_2 C_2$: phase lag

Three-term (PID) Controller

- Controller $G_c(s)$ is used to improve the closed-loop system performance.

$$G_c(s) = K_p + \frac{K_i}{s} + K_d s$$



PD Control & Phase-Lead Compensator

- *Proportional (P) + Derivative (D) Controller.*

$$G_c(s) = K_p + K_d s$$

Phase-Lead Compensator \longrightarrow $G_c(s) = K \frac{1 + \alpha Ts}{1 + Ts} \quad (\alpha > 1)$

when T is very small and αT is in a reasonable size

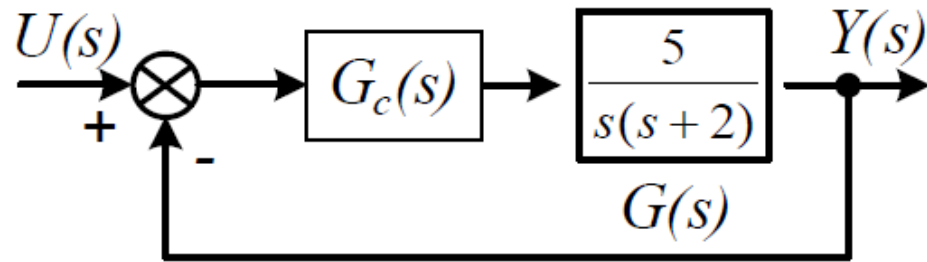
$$G_c(s) = K \frac{1 + \alpha Ts}{1 + Ts} \approx K \frac{1 + \alpha Ts}{1} = K + K\alpha Ts = K_p + K_d s$$

PD controller is an extreme case of phase-lead compensator

Disk drive control system improvement – PD controller

Design requirements: for a unit step input

$$e_{ss} = 0 \quad PO \leq 2\% \quad t_s \leq 0.08s$$



$$G_c(s) = K_p + K_d s$$

$$T(s) = \frac{5 \frac{K_p + K_d s}{s(s+20)}}{1 + 5 \frac{K_p + K_d s}{s(s+20)} \times 1} = \frac{5K_p + 5K_d s}{s(s+20) + 5K_p + 5K_d s}$$

$$T(s) = \frac{5K_p + 5K_d s}{s^2 + (20 + 5K_d)s + 5K_p}$$

Disk drive control system improvement – PD controller

$$e_{ss}=0 \quad PO \leq 2\% \quad t_s \leq 0.08s$$

$$PO = \exp\left(-\frac{\pi\zeta}{\sqrt{1-\zeta^2}}\right) = 0.02 \Rightarrow \zeta = \sqrt{\frac{(\ln(0.02))^2}{(\ln(0.02))^2 + \pi^2}} = 0.7797$$

$$t_s = \frac{4}{\zeta\omega_n} = 0.08 \Rightarrow \omega_n = \frac{4}{\zeta t_s} = 64.127$$

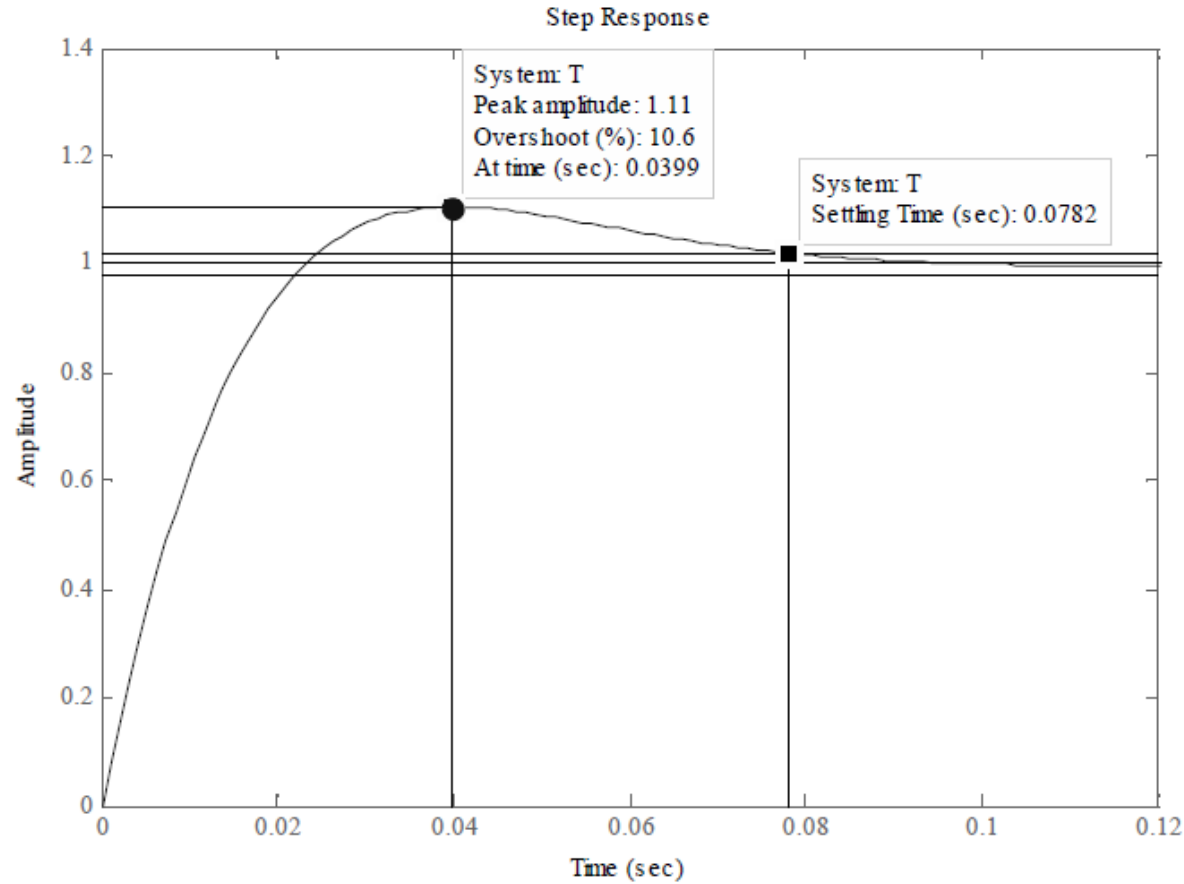
$$s^2 + (20 + 5K_d)s + 5K_p = 0 \Leftrightarrow s^2 + 2\zeta\omega_n s + \omega_n^2 = 0$$

$$5K_p = \omega_n^2 \Rightarrow K_p = \frac{\omega_n^2}{5} = 822.45$$

$$20 + 5K_d = 2\zeta\omega_n \Rightarrow K_d = \frac{2\zeta\omega_n - 20}{5} = 16$$

Disk drive control system improvement – PD controller

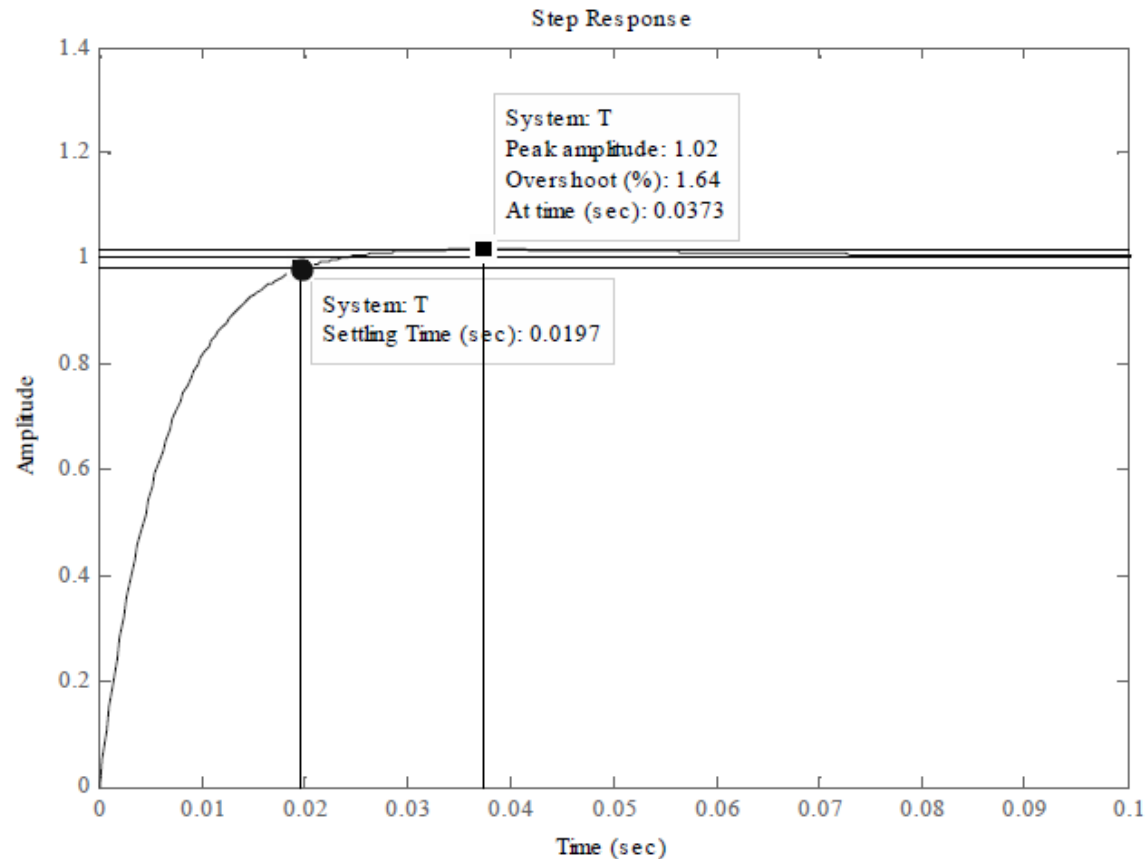
$$e_{ss} = 0 \quad PO \leq 2\% \quad t_s \leq 0.08s$$



PO bigger than the design because the effect of zero.

Disk drive control system improvement – PD controller

$$e_{ss} = 0 \quad PO \leq 2\% \quad t_s \leq 0.08s$$



$$K_p = 822.45$$

$$K_d = 32$$

Tweak K_d value to achieve the design requirement.