

Section 3.8 Book

The primary influence of damping on oscillatory systems is that of limiting the amplitude of response at resonance.

In the case of viscous damping
The amplitude at resonance is

$$X = \frac{F_0}{c\omega_n}$$

For other types of damping, no such simple expression exists.

Instead we can use an equivalent form of viscous damping (called c_{eq})

Using the dissipated energy in the system and equating it with the dissipated energy by viscous damping we have:

$$W_d = \pi c_{eq} \omega X^2$$

Then W_d must be evaluated for the system.

Example (3.8-1)

Find the equivalent damping for resistive force due to drag acting on an oscillatory system.

Assume the damping force:

$$F_d = \pm a \dot{x}^2 \quad (\text{speed } 3 \text{ to } 20 \frac{\text{m}}{\text{s}})$$

Assume harmonic motion:

$$x = -X \cos \omega t$$

$$\dot{x} = X \omega \sin \omega t$$

$$\rightarrow \frac{dx}{dt} = X \omega \sin \omega t$$

The dissipated energy in each



$$dx = (X \omega \sin \omega t) dt$$

cycle:

$$W_d = 2 \int_{-X}^X a \dot{x}^2 dx$$

$$= 2 a \omega^2 X^3 \int_0^\pi \sin^3 \omega t d(\omega t)$$

$$= \frac{8}{3} a \omega^2 X^3$$

$$W_d = \pi c_{eq} \omega X^2$$

$$\frac{8}{3} a \omega^2 X^3 = \pi c_{eq} \omega X^2$$

$$c_{eq} = \frac{8}{3\pi} a \omega X$$

The amplitude at resonance is found by substituting $c = c_{eq}$ in Eq (3.8-1) Book with $\omega = \omega_n$

$$X = \sqrt{\frac{3\pi F_0}{8a\omega_n^2}}$$

Example (3.8-2)

Find the equivalent damping for coulomb damping.

Assume the motion as $x = X \sin \omega t$
Work done per cycle by the coulomb force F_d is equal to

$$W_d = F_d (4X)$$

Substitute:

$$W_d = \pi c_{eq} \omega X^2$$

$$4 F_d X = \pi c_{eq} \omega X^2$$

$$c_{eq} = \frac{4 F_d}{\pi \omega X}$$

The amplitude of forced vibration can be found by substituting c_{eq} into Eq. (3.1-3) Book

$$X = \frac{F_0}{\sqrt{(k - m\omega^2)^2 + \left(\frac{4 F_d \omega}{\pi \omega X} \right)^2}}$$

solving for X:

$$|x| = \frac{\sqrt{F_0^2 - \left(\frac{4F_d}{\pi}\right)^2}}{K - m\omega^2}$$

$$= \frac{F_0}{K} \frac{\sqrt{1 - \left(\frac{4F_d}{\pi F_0}\right)^2}}{1 - \left(\frac{\omega}{\omega_n}\right)^2}$$

$\omega = \omega_n \rightarrow |x| \rightarrow \infty$ Not realistic

$$\frac{4F_d}{\pi F_0} < 1$$

(3.9) structural Damping

In structures, for example metals such as steel or aluminum.

the energy is dissipated proportionally

to the amplitude of vibration.

Energy dissipated by structural damping can be written as:

$$W_d = \alpha X^2$$

where α is a constant.

using the equivalent damping:

$$\pi C_{eq} \omega X^2 = \alpha X^2$$

$$C_{eq} = \frac{\alpha}{\pi \omega}$$

viscous damping, the equation of

motion is $m\ddot{x} + c\dot{x} + kx = F_0 \sin \omega t$

For structural damping, the equation

is:

$$m\ddot{x} + \left(\frac{\alpha}{\pi W}\right)\dot{x} + Kx = F_0 \sin \omega t$$

Complex stiffness.

In case of flutter, speeds of airplane wings and tail surfaces, the concept of complex stiffness is used.

For harmonic oscillations; the equation of motion can be written by:

$$m\ddot{x} + \left(K - i \frac{\alpha}{\pi}\right)x = F_0 e^{i\omega t}$$

↓
Stiffness

If we use $\gamma = \alpha / \pi K$

$$m\ddot{x} + \underbrace{K(1 + i\gamma)}_{\text{Complex stiffness}} x = F_0 e^{i\omega t}$$

γ is the structural damping factor.

Assume the solution as

$$x = \bar{X} e^{i\omega t}$$

the steady-state amplitude from

Eq. (3.9-4) becomes

$$\bar{X} = \frac{F_0}{(K - m\omega^2) + i\gamma K}$$

The amplitude at resonance is ($\omega = \omega_n$)

$$|\bar{X}| = \frac{F_0}{\gamma K}$$

Remember For viscous damping

Case:
$$|x| = \frac{F_0}{2\zeta K}$$

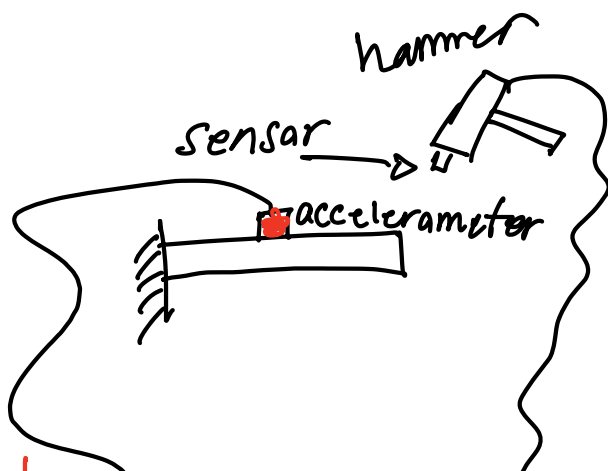
Aeroelasticity very theoretical
too many coefficient
similar to δ .

sharpness of resonance

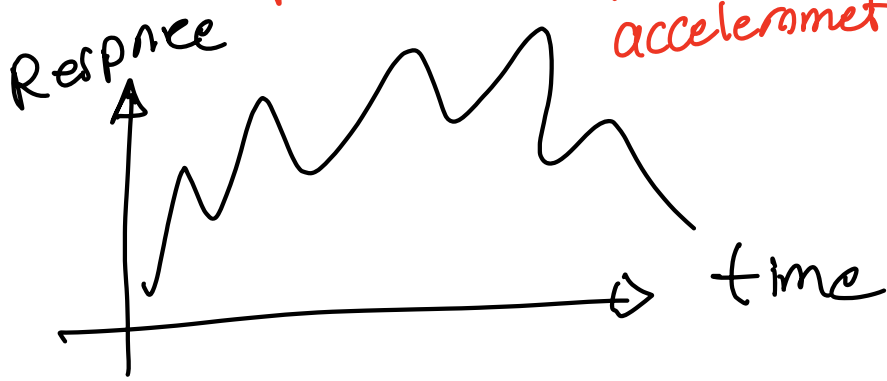
In force vibration :

using an impact using an instrumented

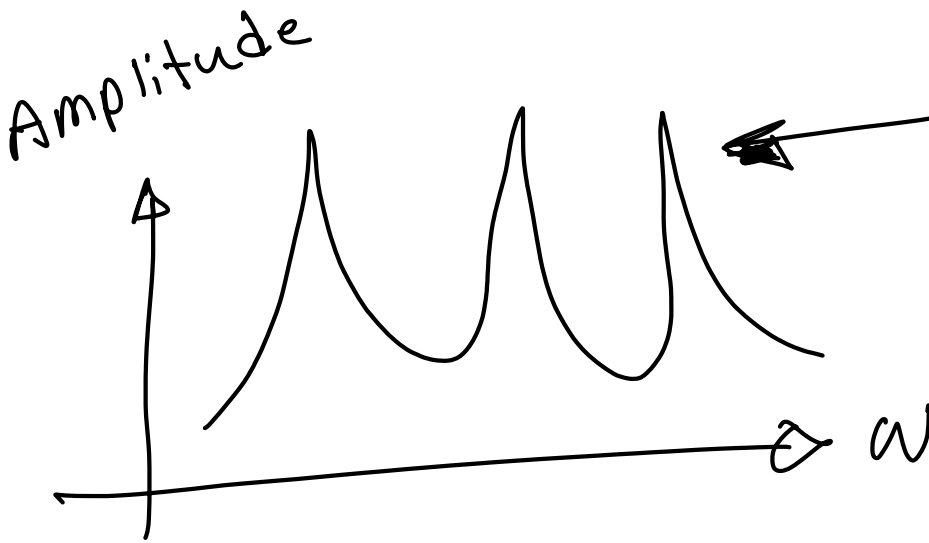
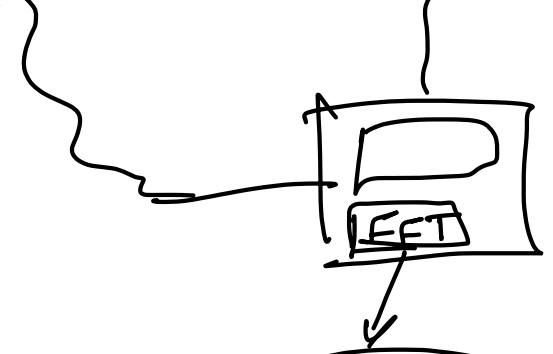
hammer
or a shaker



The response of the



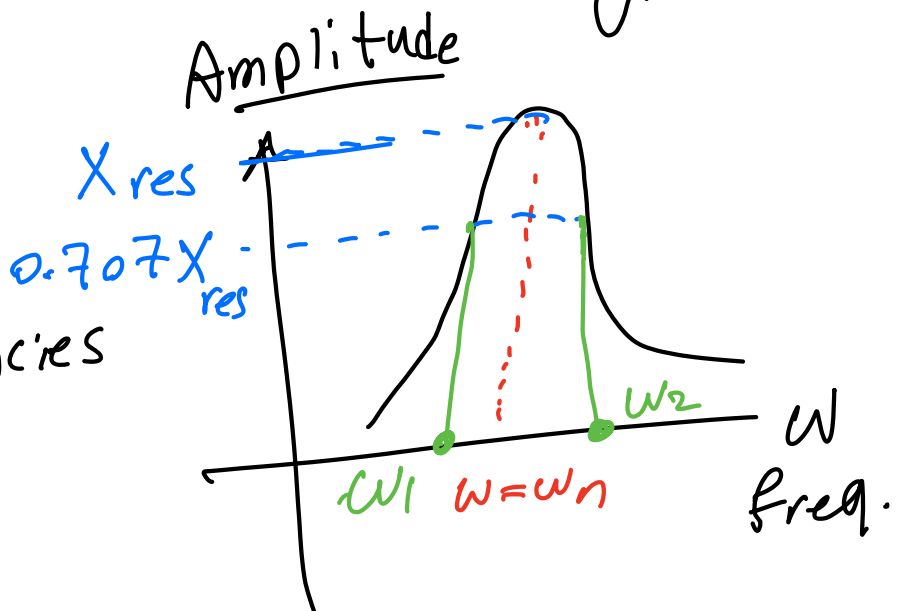
accelerometer



Fast Fourier transform

When $\omega = \omega_n$ the resonant amplitude is
$$X_{res} = \frac{(F_0/k)}{2\zeta}$$

We now seek the two frequencies on either side of resonance.



often called side bands

where $X = 0.707 X_{res}$

substitute in equation 3.1-7

and square both sides

$$\frac{1}{2} \left(\frac{1}{2f} \right)^2 = \frac{1}{\left[1 - \left(\frac{\omega}{\omega_n} \right)^2 \right]^2 + \left[2f \left(\frac{\omega}{\omega_n} \right) \right]^2}$$

$$\left(\frac{\omega}{\omega_n} \right)^2 - 2(1 - f^2) \left(\frac{\omega}{\omega_n} \right)^2 - (1 - 8f^2) = 0$$

solve for $\left(\frac{\omega}{\omega_n} \right)^2$

$$\left(\frac{\omega}{\omega_n} \right)^2 = (1 - 2f^2) \pm 2f \sqrt{1 - f^2}$$

Assuming $f \ll 1$ and therefore

structural

$$1 \gg (0.05)^2$$

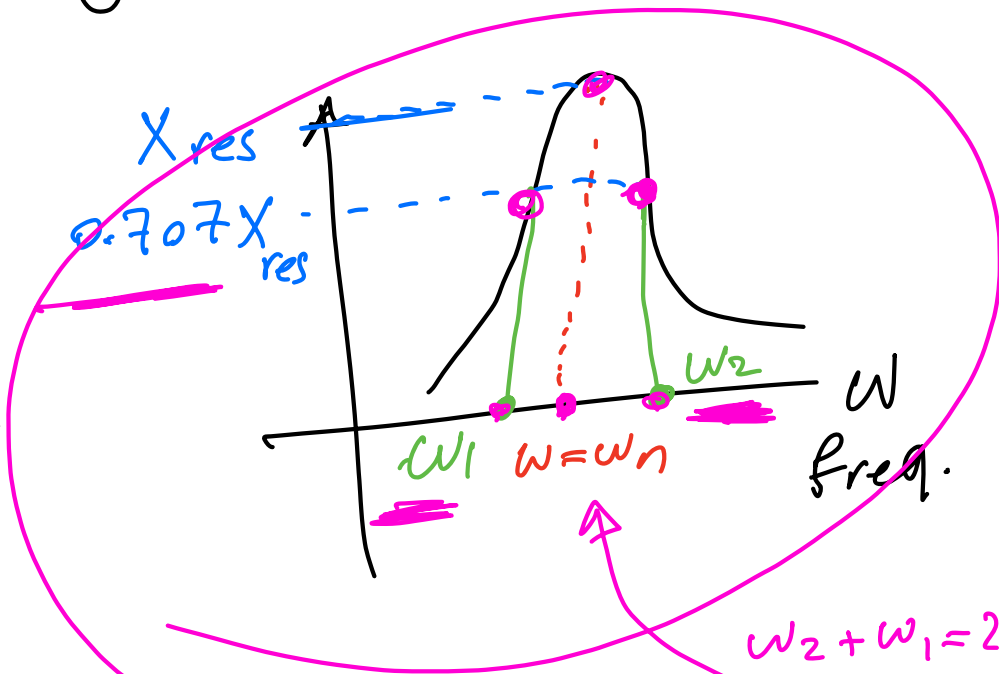
5% Damping

$$\left(\frac{\omega}{\omega_n}\right)^2 = 1 \pm 2\zeta$$

$(3 \cdot 10^{-3})$

Car damper 30%

Letting the two frequencies corresponding to the roots of Eq. (3.10.3) be ω_1 and ω_2



$$\omega_2 + \omega_1 = 2\omega_n$$

$$\omega_n = \frac{\omega_1 + \omega_2}{2}$$

$$4\zeta = \frac{\omega_2^2 - \omega_1^2}{\omega_n^2} = \frac{(\omega_2 - \omega_1)(\omega_2 + \omega_1)}{\omega_n^2}$$

$$4\zeta = 2 \left(\frac{\omega_2 - \omega_1}{\omega_n} \right) \Rightarrow \zeta = \frac{1}{2} \left(\frac{\omega_2 - \omega_1}{\omega_n} \right)$$